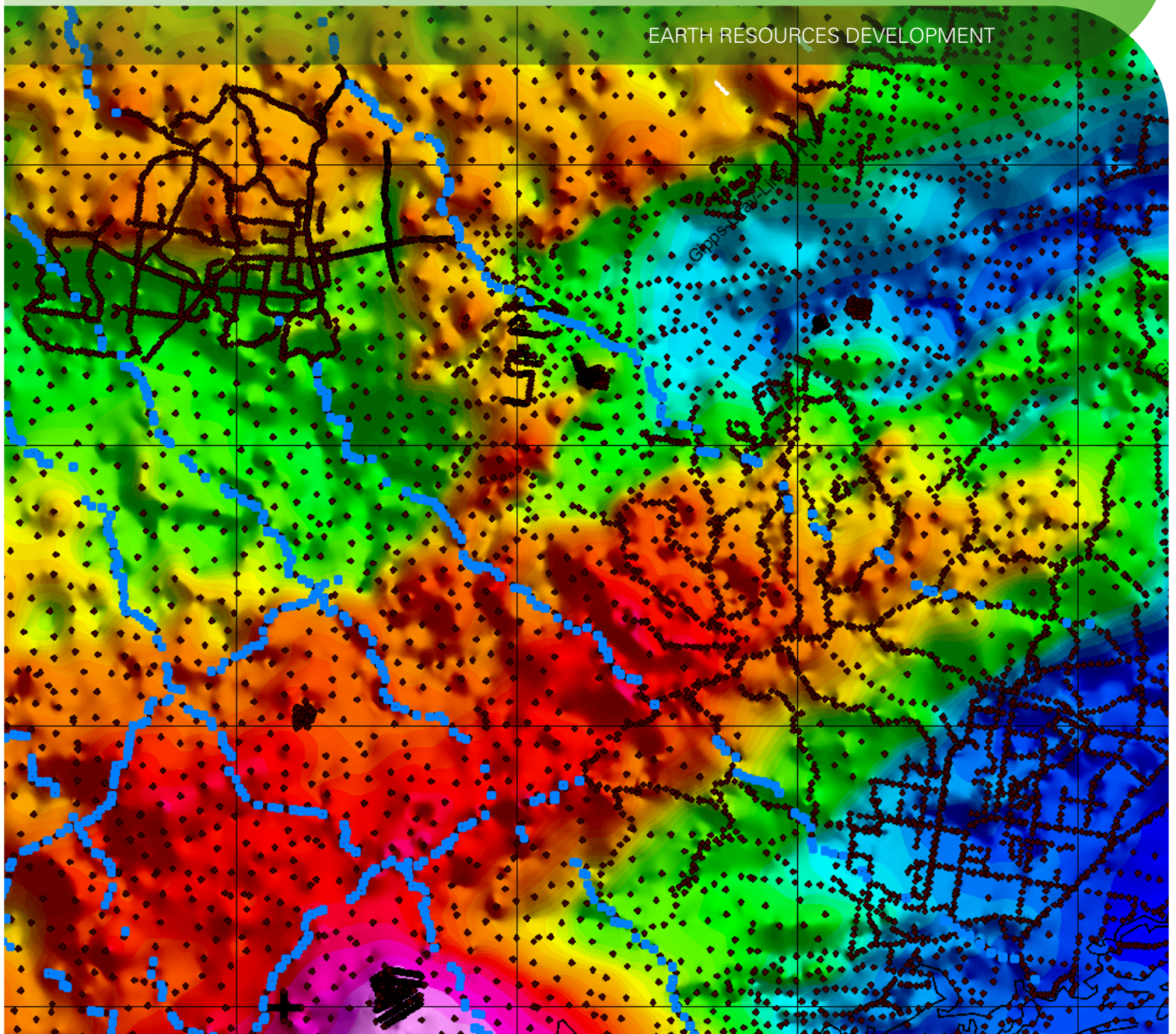


# Gippsland Basin Gravity Survey

Mathews, L.R., and McLean, M.A.

Geological Survey of Victoria Technical Record **2015/1**



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## **Keywords:**

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## **Front cover illustration:**

Bouguer anomaly grid over the Strzelecki Ranges of newly acquired gravity data integrated with pre-existing gravity data.

# Contents

<b>Executive Summary</b>	<b>5</b>
<b>1 Introduction</b>	<b>6</b>
1.1 Location and Access	6
1.2 Survey Configuration	6
<b>2 Equipment and instrumentation</b>	<b>9</b>
2.1 GPS Glonass receiver equipment	9
2.2 Gravity instrumentation	9
2.3 Other equipment	9
<b>3 Survey methodology</b>	<b>11</b>
3.1 Gravity and GPS control establishment	11
3.2 GPS data acquisition, processing and quality analysis	11
3.3 Gravity data acquisition, processing and quality analysis	14
<b>4 Results</b>	<b>21</b>
4.1 Survey timing and production rates	21
4.2 Data formats	21
4.3 Data and cross survey repeatability	22
4.4 Grids, images and plots	24
<b>Appendix A - Primary control stations</b>	<b>26</b>
<b>Appendix B - Gravity control ties</b>	<b>28</b>
<b>Appendix C - Gravity meter calibration data</b>	<b>29</b>
<b>Appendix D - Repeat gravity data</b>	<b>31</b>
<b>Appendix E - Longman's earth tide correction formula</b>	<b>34</b>
<b>Appendix F - Data formats and metadata</b>	<b>35</b>



# Executive Summary

The geometry of the Cretaceous Strzelecki Group in the Gippsland region and the underlying Palaeozoic basement of the Melbourne Zone are unresolved. The current coverage of land based gravity data in the onshore Gippsland Basin is approximately 1500 m. This resolution is not detailed enough to sufficiently characterise the geometry of the Strzelecki Group.

This project involved the acquisition of more closely spaced gravity data (500 m), placed along a series of profile lines. Specifically, the Geological Survey of Victoria (GSV) has acquired 12 regional gravity transects – 3 in a northeast orientation, and 9 in a northwest orientation – strategically located to maximise our understanding of this region's geological structures. The transects (Figures 1a & 1b) cover areas located on the Healesville, Western Port, Warragul, Moe, Traralgon, Woolamai, Wonthaggi, Foster and Yarram 1:100 000 map sheets; an area of 8,358 km<sup>2</sup>.

When combined with petrophysical data such density measurements made both from surface outcrops and also from drill core, the newly acquired gravity will be used to construct both two, and three dimensional models. Calibration with a planned 2D seismic survey across the region will further increase confidence in gravity modelling outputs. These models provide a framework which can be used to make depth to basement estimates, but most importantly, to perform hydrodynamic flow scenarios to assess the behaviour of the groundwater system in response to possible onshore natural gas development within the Gippsland Basin.

# 1 Introduction

Atlas Geophysics were contracted to acquire and process 1,213 new regional gravity stations by Geoscience Australia (GA) on behalf of the Geological Survey of Victoria (GSV). Acquisition was carried out by a 2-person crew in a vehicle along existing roads and tracks within the Gippsland Basin in south-eastern Victoria. The survey commenced on 1st July 2014 and was completed on 21st July 2014.

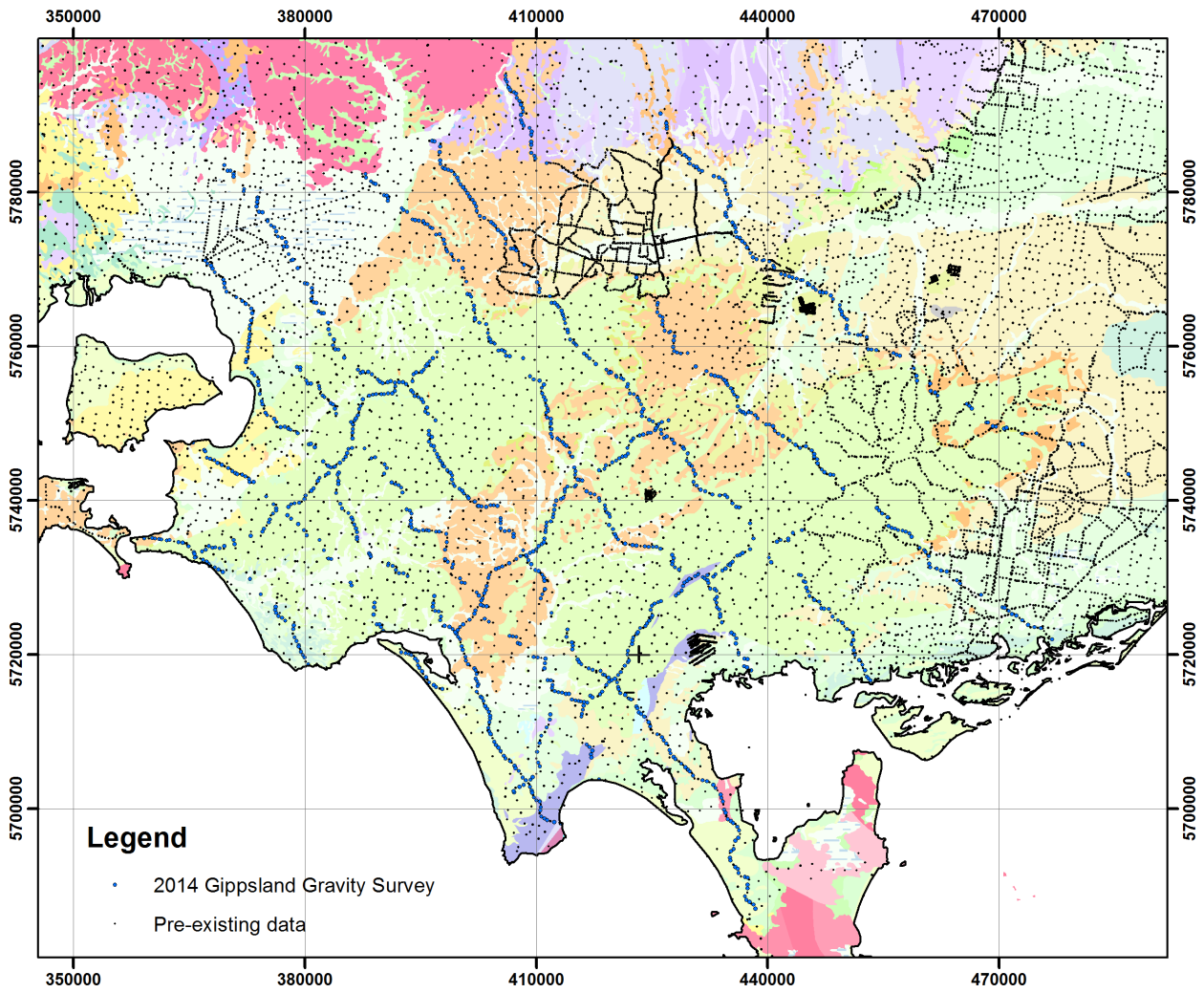
The objective of the project was to collect more gravity data to maximise our understanding of the geometry and internal structure of the Cretaceous sequence and the underlying crustal architecture of the region. When combined with density data the newly acquired gravity will be used to construct 2D models and depth estimates. Calibration with a planned 2D seismic survey across the region will increase confidence in gravity modelling outputs.

## 1.1 Location and Access

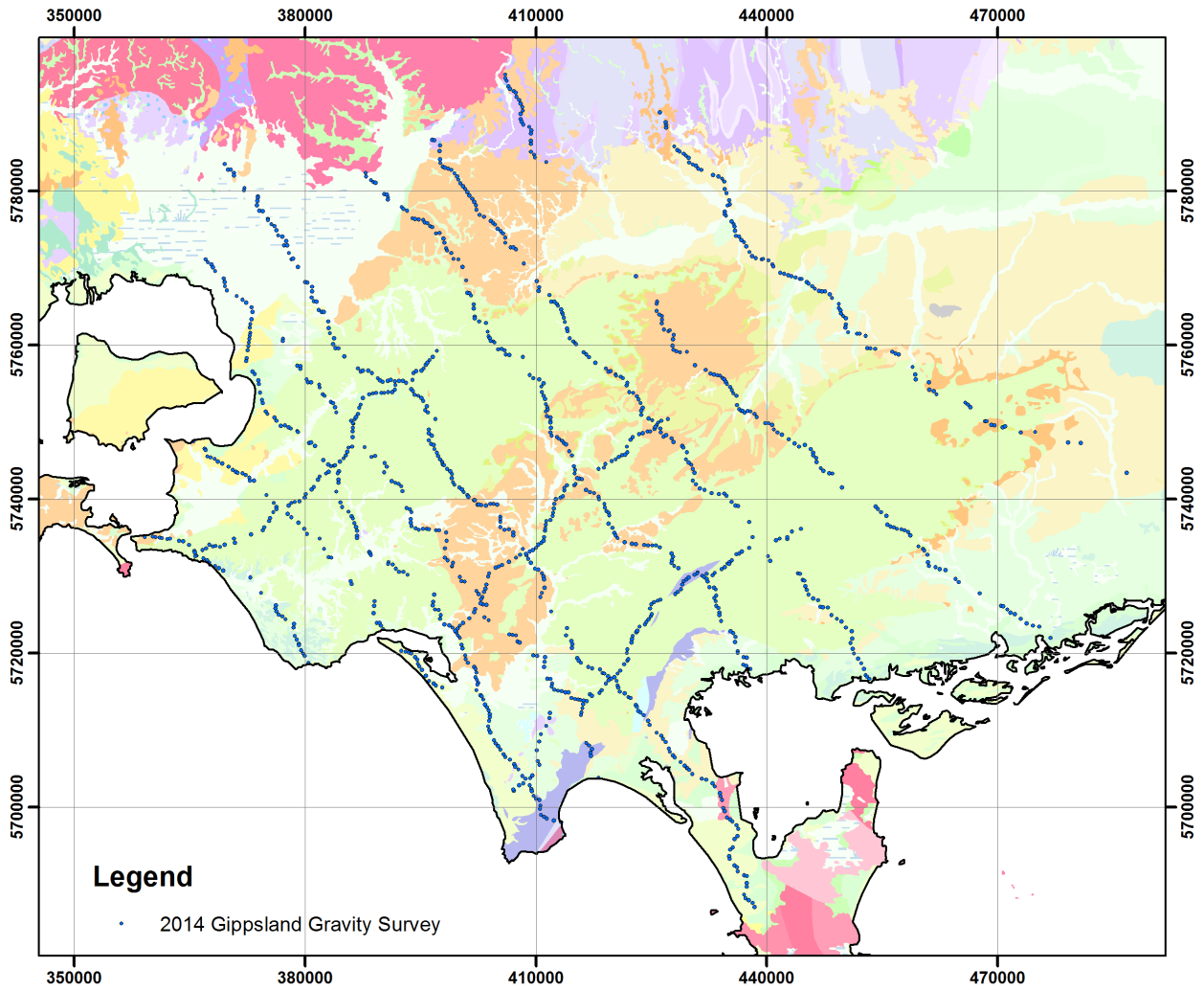
The gravity survey covered an area of approximately 8,358 km<sup>2</sup> within the Gippsland Basin in south-east Victoria (Figure 1). The crew utilised a single logistical base at Korumburra, in the northern part of the survey area. Most surveying was in open, farmland areas, but some surveying was conducted in heavily forested areas requiring longer GPS occupation times. On busy roads, traffic noise necessitated longer gravity observation times to stack out noise.

## 1.2 Survey Configuration

Gravity acquisition was conducted on existing roads and tracks on a nominal 500 m spacing according to a pre-defined survey plan outlined by the GSV. A small percentage of stations were offset or omitted from the survey where vehicular access was poor, or where tracks were fenced off due to private property. All gravity data were collected along a total of 12 profile lines – 3 in a northeast orientation, and 9 in a northwest orientation (Figures 1a & 1b). No new data were collected where previously acquired data is sufficiently detailed. Therefore, some of the northeast trending lines appear minimal, however they will be bolstered with pre-existing data during the modelling phase of the project.



**Figure 1a** Newly acquired land based gravity data (blue) and pre-existing data (black) in the onshore Gippsland Basin overlaid on the Surface Geology of Victoria 1:250000 map (2011).



**Figure 1b** Newly acquired land based gravity data in the onshore Gippsland Basin overlaid on the Surface Geology of Victoria 1:250000 map (2011).



# 2 Equipment and instrumentation

## 2.1 GPS Glonass receiver equipment

Leading edge dual-frequency GPS technologies from Leica Geosystems such as the Leica GS14 have been utilised on the project to allow for real-time kinematic (RTK) centimetre level accuracy 3D positions. The GS14 system is equipped with future proof GNSS technology which is capable of tracking all available GNSS signals including the currently available GLONASS. These new generation receivers, in conjunction with full GNSS tracking and processing, offer a new level of unmatched solution accuracy and reliability, especially when compared to existing conventional L1, L2 GPS technologies.

The use of Glonass technology in addition to GPS provides very significant advantages:

- markedly increased spatial distribution of visible satellites
- reduced horizontal and vertical Dilution of Precision (DOP) factors
- improved post-processed-kinematic (PPK) performance
- decreased occupation times means faster acquisition.

A single Leica GS14 receiver was used to conduct the survey with the receiver connecting to the Leica SmartNet Virtual Reference Station (VRS) network via Telstra Next G.

## 2.2 Gravity instrumentation

Complementing the GNSS/GPS technologies is a Scintrex CG-5 gravity meter (Figure 2). The CG-5 digital automated gravity meter offers all of the features of the low noise industry standard CG-3M micro-gravity unit, but is smaller and lighter. It also offers improved noise rejection. By constantly monitoring tilt sensors electronically, the CG-5 automatically compensates for errors in gravity meter tilt. Due to a low mass and the excellent elastic properties of fused quartz, tares are virtually eliminated.

The CG-5 can be transported over very rough terrain, on quad bikes, foot, vehicle or helicopter without taring or drifting. In terms of repeatability, the CG-5 outperforms all existing gravity meter technologies, with a factory quoted repeatability of better than 0.005 mGal. A single gravity meter was used on the project (Table 1).

**Table 1: Gravity meters used on the project**

Gravity meter type	Gravity meter code	Gravity Meter Serial Number
Scintrex CG5	A3	40269

## 2.3 Other equipment

Atlas Geophysics utilised the following additional equipment to fully support the operations:

- two HP laptop computers for data download and processing
- personal Protective Equipment for all personnel
- batteries, battery chargers, solar cells, UPS System
- survey consumables
- tools, engineering and maintenance equipment for vehicle servicing
- first aid and survival kits
- tyres and recovery equipment
- two satellite tracking and communication devices.



## SPECIFICATIONS

### Sensor Type

Fused Quartz using electrostatic nulling

### Reading Resolution

1 microGal

### Standard Field Repeatability

< 5 microGal

### Operating Range

8,000 mGal without resetting

### Residual Long-Term Drift (static)

Less than 0.02 mGal /day

### Range of Automatic Tilt Compensation

±200 arc sec

### Tares

Typically less than 5 microGals for shocks up to 20G

### Automated Corrections

Tide. Instrument Tilt Temperature. Noisy Sample. Seismic Noise Filter

### Dimensions

31 cm (H) x 22 cm x 21

### Weight (including batteries)

8 kg

### Battery Capacity

2 x 6Ah (10.8V) rechargeable Lithium-Ion Smart Batteries Full day operation in normal survey conditions with two fully charged batteries

### Power Consumption

4.5 Watts at 25°C

### Standard Operating Temperature Range

-40°C to +45°C

### Ambient Temperature Coefficient

0.2 microGal/°C (typical)

### Pressure Coefficient

0.15 microGal/kPa (typical)

### Magnetic Field Coefficient

1 microGal/Gauss (typical)

### Memory

Flash Technology (data security) Standard 12 MBytes

### Digital Data Output

RS-232 C and USB interface Is optimized for Win XP™

### Analog Data Output

Strip-Chart Recorder

### Display Screen

¼ VGA 320 x 240 pixels

### Keypad

27 key alpha/numeric

### Standard System

- CG-5 Console
- Tripod base
- 2 rechargeable batteries
- Battery Charger, 110/240 V
- External Power 110/240 V
- RS-232 and USB Cables
- Carrying Bag
- Data dump and utilities software
- Operating Manual (CD)
- Transit Case

### GPS

Ensues station referencing from an external 12 channel smart GPS antenna being connected via the RS-232 port Standard GPS accuracy <15m DGPS (WAAS) < 3m. Client has the option to use other higher accuracy GPS receivers outputting NMEA data string through the serial port.

## OPTIONS

### High Temperature Option

For use in climates that may exceed the normal operating temperature of 45°C. Allows operating temperatures of up to 55°C This option is intended to be used in climates above freezing and needs to be ordered at the time of purchase.

### Battery Belt

Suggested for cold weather operation

## COMPLETE GRAVITY SOLUTIONS

### Special Applications

Please consult LRS Scintrex or your local representative

### Training Programs

LRS Scintrex can provide training programs at our office in Canada or at your location

### Application Software

LRS Scintrex can provide software packages to support your data processing interpretation and mapping needs

An ISO 9001 2000 registered company

- \* All specifications are subject to change without notice

Figure 2 Scintrex CG5 specifications

# 3 Survey methodology

All gravity data were acquired using Atlas Geophysics Pty Ltd vehicle-borne techniques. These techniques, which involve concurrent GPS and gravity acquisition, allow for rapid acquisition of very high quality data.

## 3.1 Gravity and GPS control establishment

A single gravity control station was established near to the logistical base (Table 2). As all positional observations were made using a VRS network, it was not necessary to establish any GPS control (see Section 3.1.1)

The station was placed at the Korumburra Coal Creek toilet block (Appendix A). The station was not witnessed with an Atlas Geophysics plaque for fear of vandalism.

**Table 2: Gravity control stations used to control the survey**

Control station ID	Lat / Long / Ht (GDA94)	Observed Gravity (AAGD07 $\mu\text{m/s}^2$ )
201406500001 (GA 20140100001) Korumburra Coal Creek Toilets	-38 26 30.0700 145 49 48.7210 211.718m	9799977.70

The details of all primary control stations have been recorded on Atlas Geophysics Pty Ltd control station summary sheets. The sheets include the geodetic coordinates, observed gravity value, station description, locality sketch, locality map and a digital photo of the station. The sheets are contained in Appendix A.

### 3.1.1 Gravity control

Primary gravity control was established at the same location as the primary GPS control stations. Once tied to the Australian Fundamental Gravity Network (AFGN), the gravity control stations allowed all field gravity observations to be tied to the Australian Absolute Gravity Datum 2007 (AAGD07).

An accurate observed or absolute gravity value for the control station was established via "ABABA" ties with the project gravity meter to a nearby AFGN station. Table 3 summarises the control ties conducted and Appendix B contains the control tie data. Expected accuracy of the tie surveys would be better than 0.1  $\mu\text{m/s}^2$  (or 0.01 mGal).

**Table 3: Primary gravity control stations used to control the survey**

Control station ID	AFGN station tied to	Date of ties
201406500001 (GA 20140100001) Korumburra Coal Ck Toilets	1995901324 War Memorial Park Toilets, Drouin 1995909324 Anglican Church Hall, Drouin	14/07/2014

## 3.2 GPS data acquisition, processing and quality analysis

GPS-Glonass data were collected in real-time kinematic mode using a Leica GS14 receiver connected to the Leica SmartNet Reference Station network. This allowed for excellent GPS-Glonass ambiguity resolution and 3-D solution coordinate qualities better than 3 cm for each of the gravity station locations.

### 3.2.1 GPS-Glonass acquisition using the Virtual Reference Station Network

Each gravity station location (GSL) was positioned using navigation grade receivers running a mobile map display. At each station, the driver ensured the vehicle was always positioned safely off the road and never on a blind corner or hill crest. The vehicle was, where possible, positioned so that maximum sky coverage was achieved to minimise GPS cycle slips and record the cleanest data possible. At times, gravity station spacing was adjusted to obtain a better view of the sky and increase GPS performance.

A single GPS-Glonass receiver was used in each vehicle with the sensor mounted on the roof of the vehicle using a magnetic mount.

To acquire centimetre-level positions in real time, the crew simply connected to the VRS network via a Telstra internet connection, acquired 20 individual RTK shots, then disconnected (see 3.2.2).

### 3.2.2 Virtual Reference (VRS) Station Network

In lieu of traditional GPS-Glonass acquisition techniques which require a base station and radio links, the crew utilised the Leica SmartNet AUS Network to obtain centimetre level real-time positions. The network, covering the entire survey area, is run by Leica Geosystems Australia and consists of a network of continuously operating reference stations (CORS), and position-correcting software to provide highly accurate real-time corrections via an internet link (Figure 3).

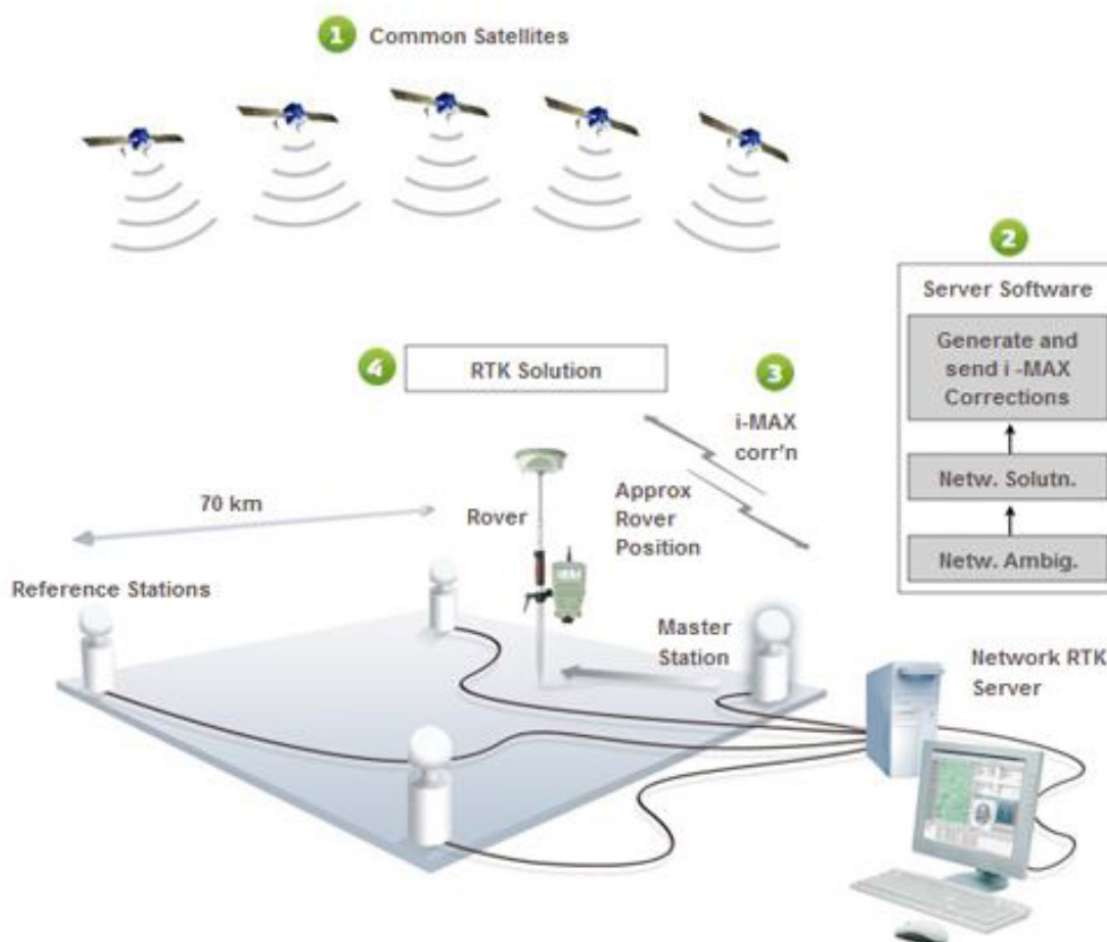


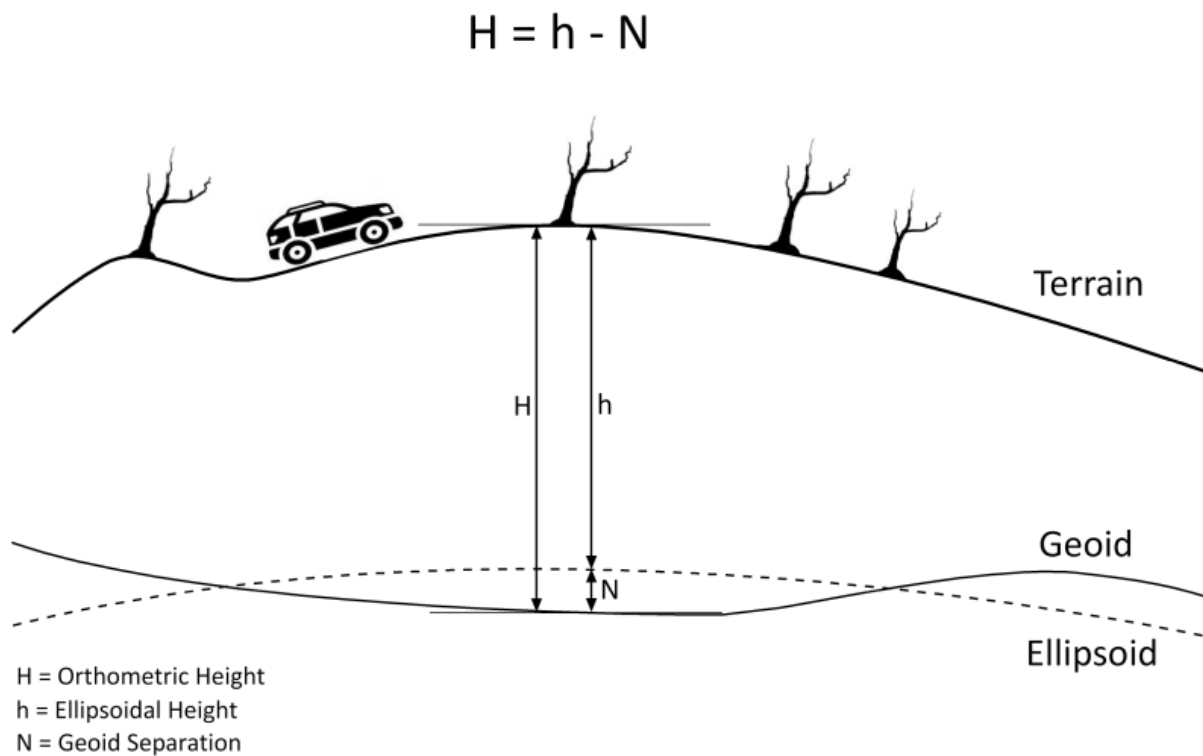
Figure 3 Leica I-Max solution

### 3.2.3 GPS-Glonass Processing

As all positional data were recorded in real time, no post processing was required other than simple projection and geoid modelling. The Leica Geo Office software suite was used to import the real time data, apply a geoid correction and projection, and then output the data into Atlas Geophysics RTK standard format. The formatted data were then imported into Atlas Geophysics data processing software "AGRIS" (Atlas Geophysics Reduction and Interpretation Software) and combined with gravity data to produce a gravity database for the project. This process was carried out on a daily basis.

Projections between GPS/Glonass derived WGS84 coordinates to Map Grid of Australia (MGA) coordinates were conducted using Leica Geo Office. For most practical applications where a horizontal accuracy of only a metre or greater is required, GDA94 coordinates can be considered the same as WGS84. MGA coordinates were obtained by projecting the GPS-derived coordinates using a Universal Transverse Mercator (UTM) projection with zone 55S. For more information about WGS84, GDA94, GRS80 and MGA coordinates, the reader is asked to visit the Geoscience Australia website: <http://www.ga.gov.au/earth-monitoring/geodesy/geodetic-datums/GDA.html>

Elevations above the Australian Height Datum (AHD) were modelled using Leica Geo Office software and the latest geoid model for Australia, AUSGEOID09. Information about the geoid and the modelling process used to extract separations (N values) can be found at <http://www.ga.gov.au/geodesy/ausgeoid/>. To obtain AHD elevation, the modelled N value is subtracted from the GPS derived WGS84/GRS80 ellipsoidal height (Figure 4).



**Figure 4** Geoid-ellipsoid separation

### 3.2.4 GPS-Glonass quality analysis

Rigorous quality analysis procedures were applied to the acquired GPS data on a daily basis using the company's in-house AGRIS (Atlas Geophysics Reduction and Information Software) software. The GPSQA module within AGRIS is used to analyse such factors as the recorded positional data, baseline distance, number of satellites, coordinate quality (CQ), standard deviation and dilution of precision (DOP) to ensure the final positional data used for gravity processing meets stringent quality specifications. Comprehensive statistics, repeatability analysis and histogram plotting are also performed.

QA procedures were applied to the GPS-Glonass data on a daily basis and any gravity stations not conforming to contract specifications were repeated.

## 3.3 Gravity data acquisition, processing and quality analysis

### 3.3.1 Calibration of the gravity meter

The gravity meters used for survey on this project were calibrated pre and post survey on the Guildford Cemetery – Helena Valley Primary School calibration range (2010990117- 2010990217) in Western Australia. The calibration process has validated the gravity meter’s scale factor to ensure reduction of the survey data produces correct observed gravity from measured dial reading values. Table 4 summarises the results of the calibration ties and lists the resultant scale factor for the survey gravity meter. Appendix C contains the reduced data used to create the summary.

**Table 4: Gravity meter scale factors**

Pre survey calibration run 27/06/2014				
Meter Code	Meter SN	Calc 2010990217 AAGD07 ( $\mu\text{m/s}^2$ )	Diff ( $\mu\text{m/s}^2$ )	Scale
A3	40269	9794484.19	0.20	1.000000

Pre survey calibration run 12/09/2014				
Meter Code	Meter SN	Calc 2010990117 AAGD07 ( $\mu\text{m/s}^2$ )	Diff ( $\mu\text{m/s}^2$ )	Scale
A3	40269	9794484.06	0.30	1.000000

Weekly tilt-tests and cycles were conducted to ensure the meter’s drift and tilt correction factors were valid. Gravity meter drift rates were monitored on a day to day basis using AGRIS software.

### 3.3.2 Acquisition of the gravity data

Gravity data were acquired concurrently with GPS-Glonass data using a Scintrex CG5 gravity meter. Data were acquired using a single loop of 10 hours duration controlled by observations at the gravity control stations. Each loop contained a minimum of two repeated readings so that an interlocking network of closed loops was formed. A total of 9.89% repeats were acquired for quality control purposes. Repeat readings were evenly distributed on a time-basis throughout each of the gravity loops.

When acquiring gravity data using a vehicle, the driver, after safely navigating to the station, parked the vehicle alongside the road in a safe position, with headlights on, rotating beacon flashing, park brake applied and vehicle engine off. Once safe to do so, the observer disembarked the vehicle on the verge or shoulder side and took the gravity reading alongside the vehicle, underneath the GPS observation point (Figure 5). At all times, the vehicle was parked on flat, level ground. Under no circumstances, did the observer acquire a reading in front of, or behind the vehicle.

At each station, the gravity operator took a minimum of two gravity readings of 60 seconds duration so that any seismic or wind noise could be detected. Control station readings were also set to 60 second duration. Before taking the reading, the operator ensured that the instrument tilt-reading was restricted to less than 5 arc-seconds and after the reading, not higher than 20 arc-seconds. Tilt-testing prior to project commencement showed that the gravity meters performed well even at extreme tilts (better than 0.01 mGal at +150/-150 arc-seconds).

If two separate readings did not agree to better than 0.02 mGal (0.01 mGal for control station readings), then the operator continued taking readings until the tolerance between consecutive readings was achieved. At the conclusion of the gravity reading, the final data display on the gravity meter was analysed to ensure the instrument was performing to specification and that the station observation provided data conforming to the project specifications. The operator also checked that the temperature, standard deviation and rejection values were within required tolerance before recording the reading. At each station, the operator recorded the gravity data digitally in the gravity meter as well as a field book so that instrument drift and reading repeatability could be analysed easily whilst in the field. Data recorded at each gravity station location was assigned a unique station code and station number.



**Figure 5 Gravity acquisition by vehicle**

Repeat stations were marked with a biodegradable flagging tape and water based marker paint for subsequent reoccupation. When reoccupying a station, the crews positioned the vehicle/walking staff as close to the original position as possible (usually better than 0.5 m). All repeat gravity observations were taken in exactly the same location.

### 3.3.3 Gravity processing

The acquired gravity data were processed using the company's in-house gravity pre-processing and reduction software, AGRIS. This software allows for full data pre-processing, reduction to Complete Bouguer Anomaly, repeatability and statistical analysis, as well as full quality analysis of the output dataset.

The software is capable of downloading Scintrex CG3/CG5 and Lacoste Romberg gravity data. Once downloaded, the gravity data is analysed for consistency and preliminary QA is performed on the data to check that observations meet specification for standard deviation, reading rejection, temperature and tilt values. Once the data is verified, the software averages the multiple readings and performs a merge with the GPS data (which it has also previously verified) and performs a linear drift correction and earth tide correction. Calculation of Free Air and Bouguer Anomalies is then performed using the contract specified formulae.

The following corrections were applied to the dataset to produce Bouguer Anomaly values for each of the gravity stations. All formulae produce values in  $\mu\text{m/s}^2$ .

#### Instrument scale factor

This correction is used to correct a gravity reading (in dial units) to a relative gravity unit value based on the meter calibration.

$$r_c = 10 \cdot (r \cdot S(r))$$

where,

- $r_c$  corrected reading in  $\mu\text{m/s}^2$
- $r$  gravity meter reading in dial units
- $S(r)$  scale factor (dial units/mGal)

### Earth Tide Correction (ETC)

The earth is subject to variations in gravity due to the gravitational attraction of the Sun and the Moon. These background variations can be corrected for using a predictive formula which utilises the gravity observation position and time of observation. The Scintrex CG5 gravity meter automatically calculates ETC but uses only an approximate position for the gravity observation so is not entirely accurate. For this reason, the Scintrex ETC is subtracted from the reading and a new correction calculated within AGRIS software. The full formula is listed in Appendix E.

$$r_t = r_c + g_{\text{tide}}$$

where,

$r_t$  tide corrected reading in  $\mu\text{m/s}^2$

$r_c$  scale factor corrected reading in  $\mu\text{m/s}^2$

$g_{\text{tide}}$  Earth Tide Correction (ETC) in  $\mu\text{m/s}^2$

### Instrument Drift Correction

Since all gravity meters are mechanical they are all prone to instrument drift. Drift can be caused by mechanical stresses and strains in the spring mechanism as the meter is moved, knocked, reset, subjected to temperature extremes, subjected to vibration, unclamped etc. The most common cause of instrument drift is due to extension of the sensor spring with changes in temperature (obeying Hooke's law). To calculate and correct for daily instrument drift, the difference between the gravity control station readings (closure error) is used to assume the drift and a linear correction is applied.

$$ID = \frac{r_{cs2} - r_{cs1}}{t_{cs2} - t_{cs1}}$$

where,

$ID$  Instrument Drift in  $\mu\text{m/s}^2$  /hour

$r_{cs2}$  control station 2nd reading in  $\mu\text{m/s}^2$

$r_{cs1}$  control station 1st reading in  $\mu\text{m/s}^2$

$t_{cs2}$  control station 2 time

$t_{cs1}$  control station 1 time

### Observed Gravity

The preceding corrections are applied to the raw gravity reading to calculate the earth's absolute gravitational attraction at each gravity station. The corrections produced observed gravity on the AAGD07 datum.

$$G_o = g_{cs1} + (r_t - r_{cs1}) - (t - t_{cs1}) \cdot ID$$

where,

$G_o$  Observed gravity in  $\mu\text{m/s}^2$

$g_{cs1}$  control station 1 known observed gravity in  $\mu\text{m/s}^2$

$r_t$  tide corrected reading in  $\mu\text{m/s}^2$

$r_{cs1}$  control station 1 reading in  $\mu\text{m/s}^2$

$t$  reading time

$t_{cs1}$  control station 1 time

$ID$  instrument drift in  $\mu\text{m/s}^2$ /hour

### Normal Gravity

The normal (or theoretical) gravity value at each gravity station is calculated based on the assumption that the Earth is a homogeneous ellipsoid. The closed form of the 1980 International Gravity Formula is used to approximate the theoretical gravity at each station location and essentially produce a latitude correction. Gravity values vary with latitude as the earth is not a perfect sphere and the polar radius is much smaller than the equatorial radius. The effect of centrifugal acceleration is also different at the poles versus the equator.

$$G_n = 9780326.7715((1+0.001931851353(\sin^2 l))/(SQRT(1-0.0066943800229(\sin^2 l))))$$

where,

$G_n$  Theoretical Gravity in gravity units

$l$  GDA94 latitude at the gravity station in decimal degrees



### Atmospheric Correction

The gravity effect of the atmosphere above the ellipsoid can be calculated with an atmospheric model and is subtracted from the normal gravity.

$$AC=8.74 - 0.00099 \cdot h + 0.0000000356 \cdot h^2$$

where,

*AC* Atmospheric correction in gravity units  
*h* elevation above the GRS80 ellipsoid in metres

### Free Air Correction

Since the gravity field varies inversely with the square of distance, it is necessary to correct for elevation changes from the reference ellipsoid (GRS80). Gravitational attraction decreases as the elevation above the reference ellipsoid increases.

$$FAC=-(3.087691 - 0.004398 \sin^2 l) \cdot h + 7.2125 \cdot 10^{-7} \cdot h^2$$

where,

*FAC* Free air correction in gravity units  
*l* GDA94 latitude at the gravity station in decimal degrees  
*h* elevation above the GRS80 ellipsoid in metres

### Bouguer Correction

If a gravity observation is made above the reference ellipsoid, the effect of rock material between the observation and the ellipsoid must be taken into account. The mass of rock makes a positive contribution to the gravity value. The correction is calculated using the closed form equation for the gravity effect of a spherical cap of radius 166.7 km, based on a spherical Earth with a mean radius of 6,371.0087714 km, height relative the ellipsoid and a rock density of 2.67 t/m<sup>3</sup>.

$$BC= 2\pi G\rho((1+\mu) \cdot h - \lambda R)$$

where,

*BC* Bouguer correction in gravity units  
*G* gravitational constant = 6.67428 x 10<sup>-11</sup> m<sup>3</sup>kg<sup>-1</sup>s<sup>-2</sup>  
*ρ* rock density (2.67 t/m<sup>3</sup>)  
*h* elevation above the GRS80 ellipsoid in metres  
*R* (*R<sub>0</sub>*+*h*) the radius of the earth at the station  
*R<sub>0</sub>* mean radius of the earth = 6,371.0087714 km (on the GRS80 ellipsoid)  
*μ* & *λ* are dimensionless coefficients defined by:

$$\mu=((1/3) \cdot \eta^2 - \eta) \cdot$$

where,

*η* *h/R*

$$\lambda = (1/3)\{(d + f\delta + \delta^2)[(f - \delta)^2 + k]^{1/2} + p + m \cdot \ln(n/(f - \delta + [(f - \delta)^2 + k]^{1/2})\}$$

where,

*d* 3·cos2α-2  
*f* cosα  
*k* sin2α  
*p* -6 · cos2α · sin(α/2) + 4 · sin3(α/2)  
*δ* (*R<sub>0</sub>*/*R*)  
*m* -3 · *k* · *f*  
*n* 2 · [sin(α/2)-sin2(α/2)]  
*α* *S/R<sub>0</sub>* with *S* = Bullard B Surface radius = 166.735 km

### **Terrain Correction**

The terrain correction accounts for variations in gravity values caused by variations in topography near the observation point. The correction accounts for the attraction of material above the assumed spherical cap and for the over-correction made by the Bouguer correction when in valleys. The terrain correction is positive regardless of whether the local topography consists of a mountain or a valley. Section 3.3.4 contains a more in-depth discussion of the terrain correction process.

### **Free Air Anomaly**

The free air anomaly is the difference between the observed gravity and normal gravity that has been computed for latitude and corrected for the elevation of the gravity station above or below the reference ellipsoid:

$$FAA = G_o - (G_n - AC) - FAC$$

where,

*FAA* Free Air Anomaly in gravity units  
*G<sub>o</sub>* Observed Gravity in gravity units  
*G<sub>n</sub>* Normal Gravity in gravity units  
*AC* Atmospheric Correction in gravity units  
*FAC* Free Air Correction in gravity units

### **Bouguer Anomaly**

The Bouguer anomaly is computed from the free air anomaly above by removing the attraction of the spherical cap calculated by the Bouguer correction.

$$BA = FAA - BC$$

where,

*BA* Bouguer Anomaly in gravity units  
*FAA* Free Air Anomaly in gravity units  
*BC* Bouguer Correction in gravity units

### **Complete Bouguer Anomaly**

This is obtained by adding the terrain correction to the Bouguer anomaly. The Complete Bouguer anomaly is the most interpretable value derived from a gravity survey as changes in the anomaly can be directly attributed to lateral density contrasts within the geology below the observation point.

$$CBA = BA + TC$$

where,

*CBA* Complete Bouguer Anomaly in gravity units  
*BA* Bouguer Anomaly in gravity units  
*TC* Terrain Correction in gravity units

## **3.3.4 Terrain Corrections**

Terrain corrections, which account for the variation in gravity due to topography proximal to the gravity station, were computed using a digital elevation model (DEM) and RASTERTC software from Geopotential. RASTERTC software permits the user to input a DEM in the form of a binary grid file, and gravity data in an ASCII file. From this information, the software is capable of calculating extremely accurate terrain corrections. For more detailed information regarding the software and algorithm, the reader is asked to visit the Geopotential website <http://geopotential.com/docs/RasterTC/RasterTC.html>

Elevation data were sourced from the 1 second SRTM Level 2 Derived Smoothed Digital Elevation Model (DEM-S) Version 1.0 which has an equivalent cell size of 30 m. Data were extracted to provide a 30 km buffer from the extents of the gravity survey. To account for bathymetry, the SRTM DEM data were merged with data from the AUSBATH\_09\_v4 coverage.

A comparison against GPS heights recorded during the gravity survey revealed that the DEM data were sufficiently accurate to be used in regional terrain corrections. The average difference between GPS height and DEM heights was -2.99 m and the standard deviation of the differences was 3.39 m. Some of the larger differences would be attributable to vegetation cover.

When executing the terrain correction, the following inputs were used with RASTERTC:

RMIN = 30 m  
 RMED = 250 m  
 RMAX = 30000 m  
 Angle = 6 degrees

RMIN was selected to enable correction for topography near to the gravity station and coincided with the grid cell size of the SRTM DEM. RMAX was selected to allow for outer zone correction of severe topography at large distances from the gravity station. RMED was chosen so that the DEM would be sampled at an interval close to the grid cell size of the DEM when using the 6 degree integration angle.

The terrain correction software provides indicators for terrain correction quality and accuracy as part of its output. The output variables QFINNER and QFOUTER specify the quality factor for each correction made. If these factors have a value of 0, then the user can assume that the terrain correction proceeded successfully. If non-zero values are reported, then the value of the QF factor will provide an indication as to possible problems or inadequacies in the correction.

For the inner zone correction, an indicator of how well the terrain in the immediate vicinity of a gravity station is represented by the available elevation samples is obtained by examining the spatial distribution of the elevation samples. In the radial interval Rmin to Rmed, RASTERTC counts the number of samples falling within the 8 octants surrounding the station. If any of these octants are missing elevation samples, that fact is noted, and the tabulated quality factor simply notes how many of the octants are missing samples (see Table 5).

For the outer zone correction, a result of 0 means that the correction proceeded successfully. If a portion of the outer-zone terrain is missing from the DEM supplied, the value of QF-Outer will reflect the per cent of terrain that was available (rounded to the nearest per cent). For example, if QF-Outer is 91, the implication is that 9% of the terrain in the outer zones was missing for some reason, and that the terrain correction calculated for that particular station is too small by some amount.

**Table 5: Terrain correction error codes**

QF-Inner	Explanation of error code
0	Inner-zone terrain calculation OK
1	No elevation samples occur in 1 octant surrounding the gravity station
2	No elevation samples occur in 2 octant surrounding the gravity station
3	No elevation samples occur in 3 octant surrounding the gravity station
4	No elevation samples occur in 4 octant surrounding the gravity station
5	No elevation samples occur in 5 octant surrounding the gravity station
6	No elevation samples occur in 6 octant surrounding the gravity station
7	No elevation samples occur in 7 octant surrounding the gravity station
22	Duplicate elevation nodes encountered while calculating terrain gradients
23	All elevation nodes collinear or triangulation structure corrupted

### 3.3.5 Quality analysis of the processed gravity data

Following reduction of the data to Bouguer Anomaly, repeatability and QA procedures were applied to both the positional and gravity observations using AGRIS software. AGRIS checks the following as part of its QA processing:

- Easting Observation Repeatability and Histogram
- Northing Observation Repeatability and Histogram
- Elevation Observation Repeatability and Histogram
- Gravity Observation Repeatability and Histogram
- Gravity SD, Tilt XY, Temperature, Rejection, Reading Variance
- Gravity meter drift / closure
- Gravity meter loop time, drift per hour
- GPS Dilution of Precision, Coordinate Quality Factor, Standard Error
- Variation of surveyed station location from programmed location.

QA procedures were applied to the gravity data on a daily basis and any gravity stations not conforming to contract specifications were repeated.

### 3.3.6 Additional processing, gridding and plotting

Complementing the QA procedures is additional daily gridding, imaging and plotting of the elevation and gravity data. Once processed to Bouguer Anomaly and assessed for QA, data are imported into Geosoft Oasis Montaj or ChrisDBF software for gridding at 1/5<sup>th</sup> the station spacing to produce ERMapper compatible grid files. Resultant grids are contoured, filtered and interpreted using ERMapper and ArcMap software to check that data is smoothly varying and that no spurious anomalies are present. A first vertical, tilt angle and horizontal derivative filter are routinely applied to the data as these filters allow for excellent noise recognition. Once identified, any spurious stations can be field checked the following day and repeated if required. During the course of the survey, two anomalous stations were field checked and found to be valid.

Plotting of the acquired stations on a daily basis allowed for identification of any missed stations which were then gained the following day.

# 4 Results

The Gippsland gravity survey was completed with relative ease despite a few issues with access where tracks did not exist, or were fenced off.

Some inclement weather and boggy conditions (in State Forest) did slow acquisition at times, as did surveying under canopy. Observations along the roadside and in sandy, soft conditions often required longer occupation times for readings to be within tolerance.

A total of 1,213 new gravity stations were gained during the survey.

Final data have been delivered to a technically excellent standard and are presented both digitally and hardcopy as Appendices to this report.

## 4.1 Survey timing and production rates

The survey crew began gravity data acquisition on Tuesday 1st July 2014 with survey cessation on Monday 21st July 2014. The only downtime experienced was due to inclement weather and a requirement to revisit roads which received a lot of traffic during peak times.

Production for the duration of the survey was good whilst surveying using vehicles with an average production of about 60 stations per day.

## 4.2 Data formats

Final point located data for the project have been delivered in ASEG-GDF2 compliant format. Appendix F contains a listing of the definition and description files accompanying the final data. Table 6 summarises the deliverables.

**Table 6: Final deliverables**

Final delivered data	Format	Data USB	Hardcopy
Gravity Database	Point located data ASEG-GDF2	•	
Raw Positional Data	AGRIS format, comma delimited	•	
Raw Gravity Data	Scintrex CG5 format	•	
Raw GPS-GNSS Data	Waypoint GPB Binary	•	
Gravity Control Data	Microsoft Excel Format	•	•
Calibration Data	Microsoft Excel Format	•	•
Repeat Data	Microsoft Excel Format	•	•
Terrain Corrections	RASTERTC output file	•	
Final Grids	ERMapper Grids .ers	•	
Final Images	GIS compatible TIFF	•	•
Acquisition Report	PDF .pdf	•	•

## 4.3 Data and cross survey repeatability

The repeatability of both the gravity and GPS data was excellent. In total, 120 gravity and GPS repeat stations were collected and analysed. As a percentage, this equates to 9.89% of the total number of new gravity stations acquired. Repeat stations were acquired so that an even distribution between gravity loops was established and that all loops were interlocked.

Descriptive statistics pertaining to the repeatability are contained in Table 7 and Appendix D contains a tabulation of the actual repeat data for the entire survey.

The standard deviation of the gravity repeat deviations was  $0.25 \mu\text{m/s}^2$  and the standard deviation of the GPS derived elevation repeat deviations was 0.038 m. These statistics confirm that the data have exceeded contract specifications.

**Table 7: Repeat statistics**

	Elevation Repeat (mGRS80)	Gravity Repeat ( $\mu\text{m/s}^2$ )
Mean	-0.003	0.01
Standard Error	0.004	0.02
Median	0.000	0.00
Mode	-0.013	0.00
Standard Deviation	0.038	0.25
Sample Variance	0.001	0.06
Kurtosis	1.166	-0.16
Skewness	-0.212	0.14
Range	0.240	1.34
Minimum	-0.117	-0.68
Maximum	0.123	0.66
Sum	-0.383	0.63
Count	120	120

### 4.3.1 Repeatability histograms

Histograms showing the distribution of repeat differences for both the GPS and gravity observations are shown in Figures 6 and 7.

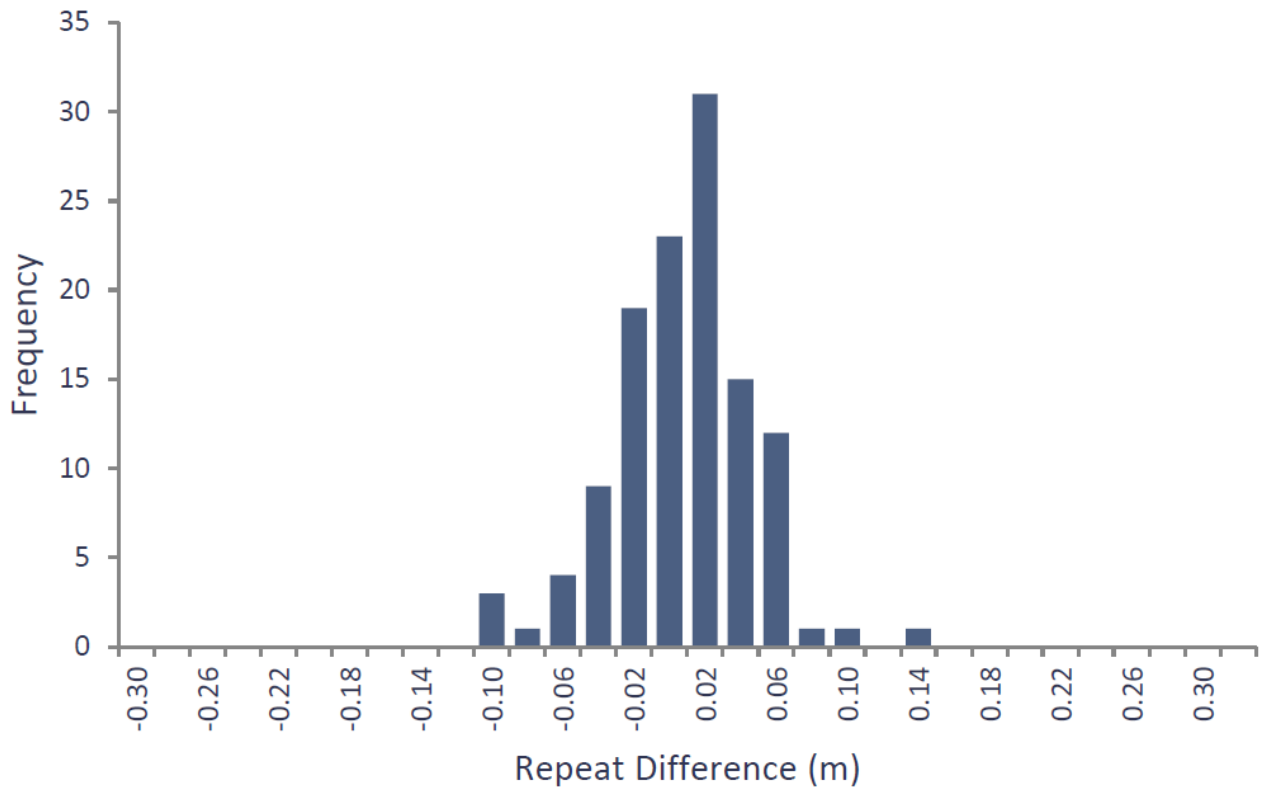


Figure 6: Histogram of elevation repeat differences

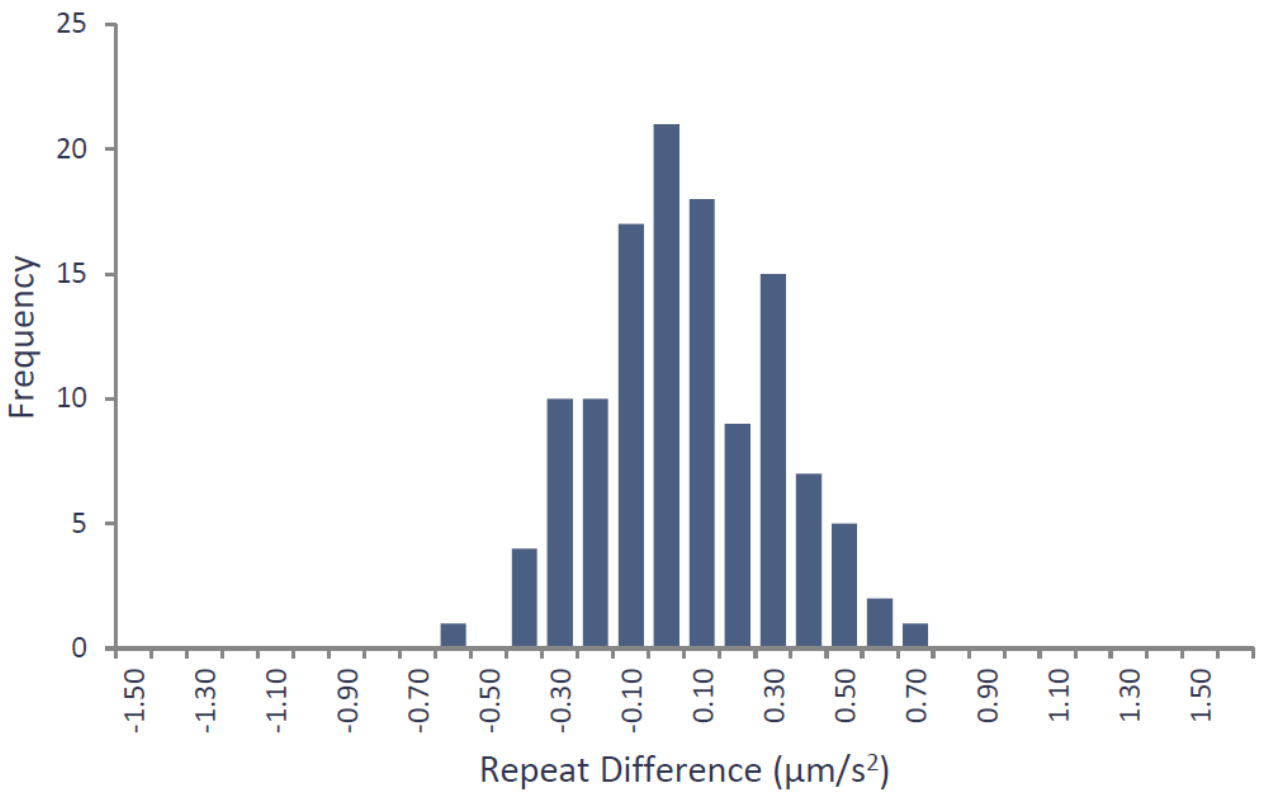
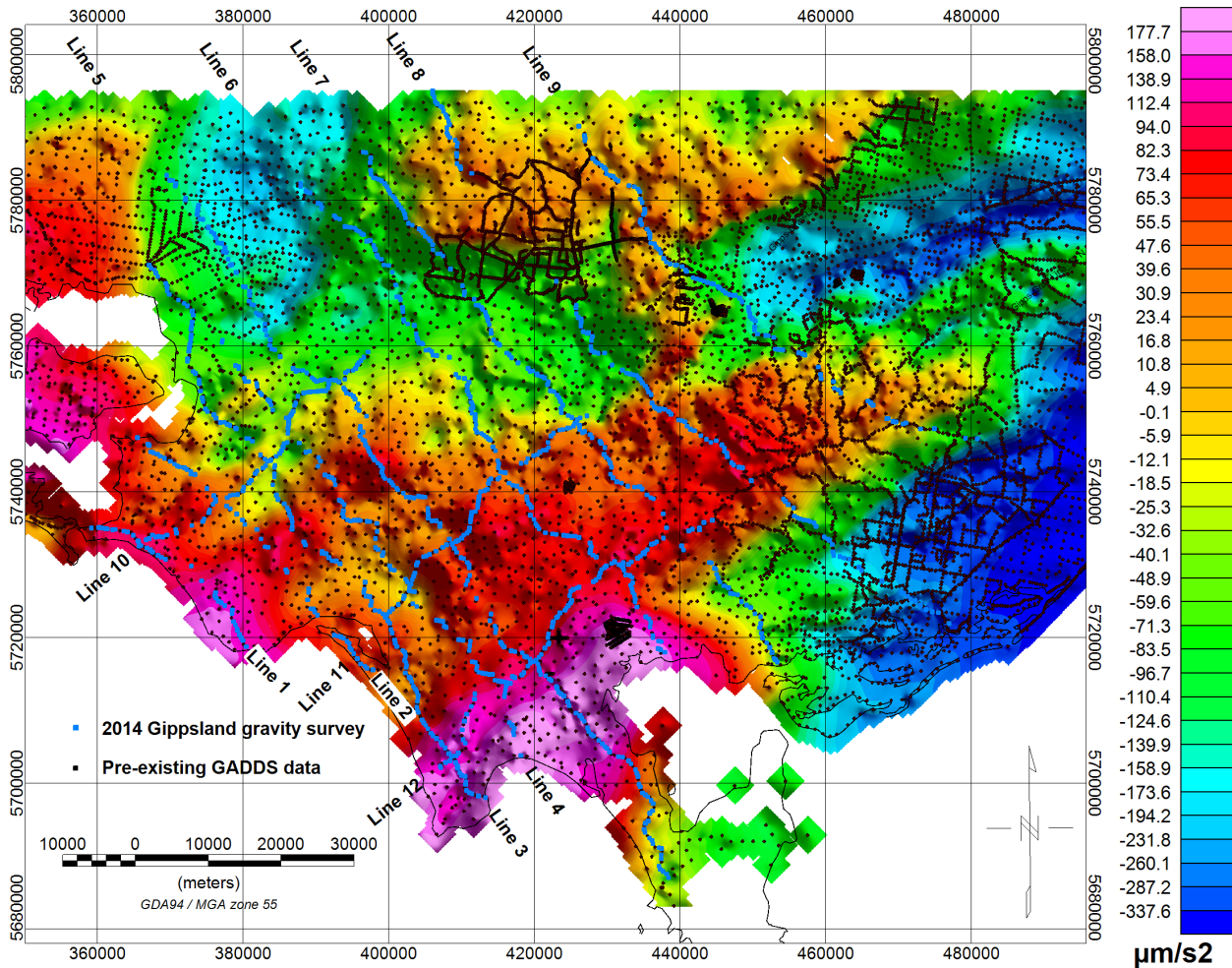


Figure 7: Histogram of gravity repeat differences

## 4.4 Grids, images and plots

Final reduced Complete Spherical Cap Bouguer Anomaly (CSCBA267) data have been integrated with the pre-existing gravity data and gridded using Geosoft Oasis Montaj software. Data have been gridded with a minimum curvature algorithm, a grid cell size of 100 m and displayed in  $\mu\text{m}/\text{s}^2$ .

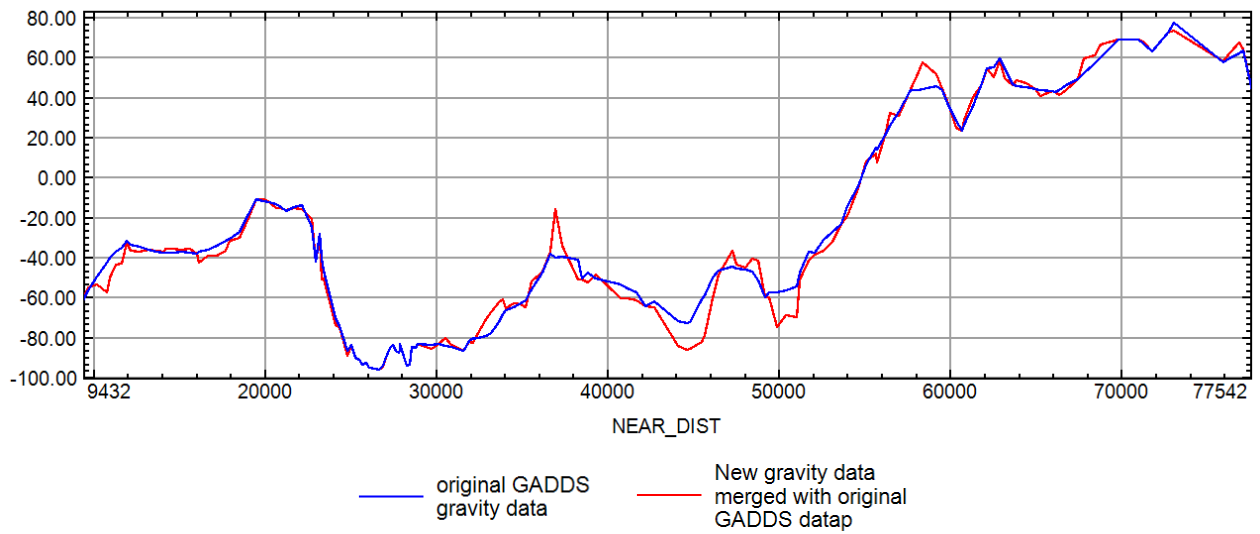


**Figure 8** Complete Spherical Cap Bouguer Anomaly (CSCBA267) of newly acquired gravity data (blue points) integrated with pre-existing gravity data (black points).

An example profile through line 7 is shown in figure 9. This figure shows that although the broad wavelength is captured by the pre-existing data, the newly acquired data has identified short wavelength variations in the gravity field which can be attributed to the geological signal.



## Gippsland gravity - line 7



**Figure 9** Profile through line 7 showing the processed Complete Spherical Cap Bouguer Anomaly (CSCBA267) values of both the pre-existing gravity data (blue), and the newly acquired gravity data integrated with pre-existing gravity data (red).

# Appendix A - Primary control stations

201406500001 (GA 20143000001) – Korumburra Coal Creek Toilets					
GDA94/GRS80		MGA Z55		AMG Z55	
Latitude	-38 26 30.0700	Easting	397,912.138	Easting	397,798
Longitude	145 49 48.7210	Northing	5,744,529.163	Northing	5,744,344
Ellipsoidal Height	211.718	Orthometric Height	207.474	Orthometric Height	207.474

## Observed Gravity

**AAGD07  $\mu\text{m/s}^2$       9799977.90**

### Occupation Method/Location Details

The gravity control point is located on a concrete slab floor abutting the northern wall of the Coal Creek toilets, Korumburra. The gravity location is centred in the middle of the wall directly under the green and white emergency assembly area sign, 0.5 m from the wall.

Gravity Control was established by Atlas Geophysics via three separate ABA loops with the project gravity meter to AFGN stations 1995901324 and 1995909324, Drouin, Victoria. Expected accuracy would be better than 0.1  $\mu\text{m/s}^2$ .

GPS Control was not established at this station, but the coordinates of the gravity base have been established with a VRS Network averaged solution accurate to better than 2cm.

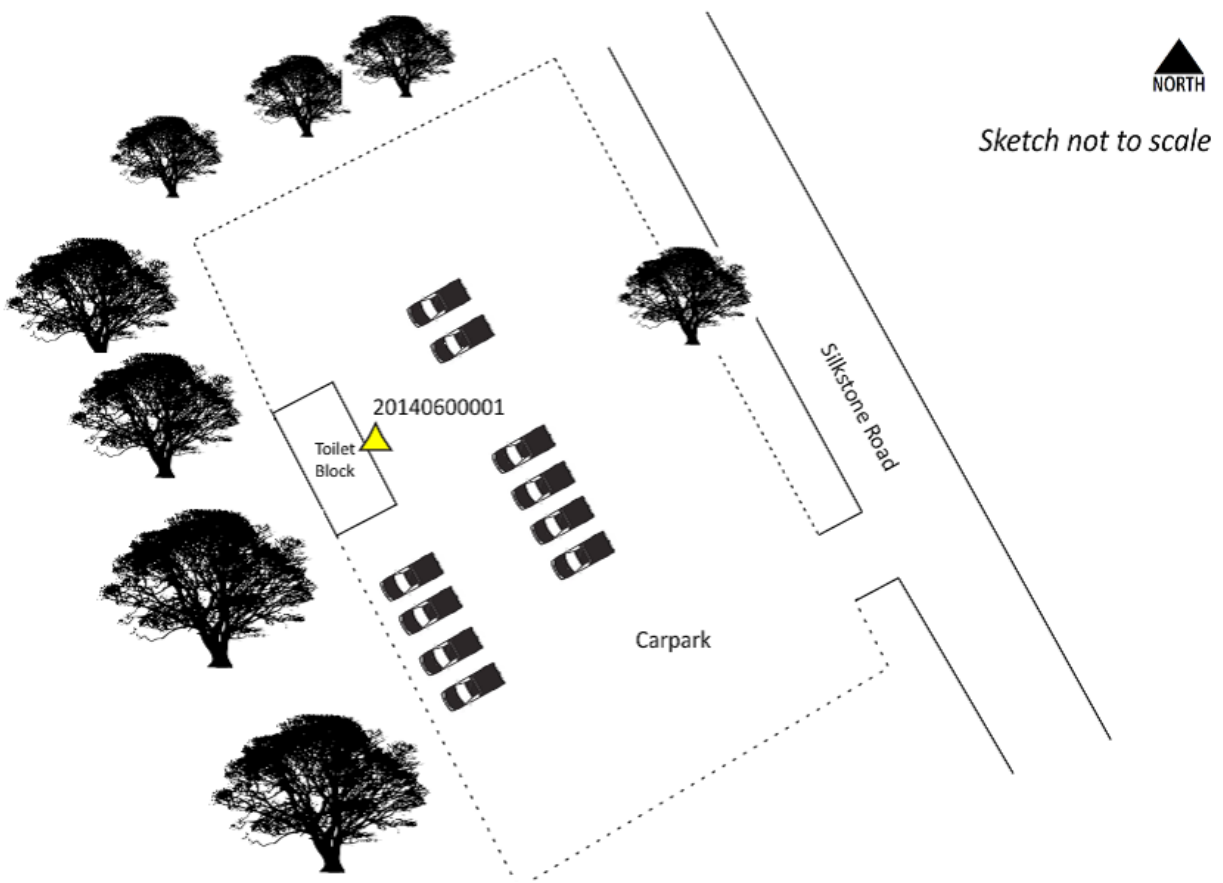
The toilet block is located 32 m south west of Silkstone Rd, Korumburra. A large gravel car park is located to the north of the toilet block and provides ample parking space.



**Photograph of Control Station 201406500001**



Location of control station 201406500001



Locality Sketch of Control Station 201406500001

# Appendix B - Gravity control ties

## 201406500001 Gravity Control Ties

1 = 201406500001 Korumburra Coal Creek Toilets

1324 = 1995901324 War Memorial Park Toilets, Drouin

9324 = 1995909324 Anglican Church Hall, Drouin

Ties carried out by vehicle

### METER A3

station	gda94_longitude_ dd	gda94_latitude_ dd	date_ ddmmyyyy	time_ hhmmss	dialrdng_ mgal	etc_ mgal	aagd07_ mgal	metersn
1	145.830200	-38.441686	14/07/2014	8:38:46	3071.628	-0.102	980000.000	40269
1	145.830200	-38.441686	14/07/2014	8:39:52	3071.626	-0.102	980000.000	40269
1324	145.856250	-38.135136	14/07/2014	10:36:27	3045.767	-0.053	979974.205	40269
1324	145.856250	-38.135136	14/07/2014	10:37:33	3045.771	-0.053	979974.210	40269
9324	145.854770	-38.133125	14/07/2014	10:56:34	3044.967	-0.042	979973.419	40269
9324	145.854770	-38.133125	14/07/2014	10:57:40	3044.966	-0.042	979973.419	40269
1	145.830200	-38.441686	14/07/2014	12:23:41	3071.493	-0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	12:24:47	3071.496	-0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	12:24:47	3071.496	-0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	12:24:47	3071.496	-0.004	980000.000	40269
1324	145.856250	-38.135136	14/07/2014	13:15:34	3045.720	0.009	979974.237	40269
1324	145.856250	-38.135136	14/07/2014	13:16:40	3045.720	0.009	979974.237	40269
9324	145.854770	-38.133125	14/07/2014	13:25:21	3044.903	0.010	979973.420	40269
9324	145.854770	-38.133125	14/07/2014	13:26:27	3044.905	0.010	979973.422	40269
1	145.830200	-38.441686	14/07/2014	14:18:33	3071.488	0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	14:19:39	3071.488	0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	14:19:39	3071.488	0.004	980000.000	40269
1	145.830200	-38.441686	14/07/2014	14:19:39	3071.488	0.004	980000.000	40269
1324	145.856250	-38.135136	14/07/2014	15:23:08	3045.744	-0.015	979974.238	40269
1324	145.856250	-38.135136	14/07/2014	15:24:14	3045.757	-0.015	979974.251	40269
9324	145.854770	-38.133125	14/07/2014	15:36:12	3044.931	-0.021	979973.419	40269
9324	145.854770	-38.133125	14/07/2014	15:37:18	3044.933	-0.021	979973.421	40269
1	145.830200	-38.441686	14/07/2014	16:46:56	3071.543	-0.056	980000.000	40269
1	145.830200	-38.441686	14/07/2014	16:46:56	3071.543	-0.056	980000.000	40269

AVG 1324 979974.241

AVG 9324 979973.420

DIFF 1324\_1 -25.759

DIFF 9324\_1 -26.580

KNOWN 1324 979972.038

KNOWN 9324 979971.202

CALC 1 1324 979997.797

CALC 1 9324 979997.782

**CALC 1** 979997.790 mGal AAGD07

**979997.90**  $\mu\text{m/s}^2$  AAGD07

# Appendix C - Gravity meter calibration data

P2014065\_GA\_Gippsland

## Pre Survey Calibration Data

1 = 2010990117 CS1 Guildford Cemetery 9793899.63  $\mu\text{m/s}^2$  AAGD07

2 = 2010990217 CS2 Helena Valley Primary School 9794483.85  $\mu\text{m/s}^2$  AAGD07

Station	MGAE	MGAN	Date	Time	OBSGAAD07_ $\mu\text{m/s}^2$	Drift_ $\mu\text{m/s}^2$	Serial
A3 METER							
1	403387.00	6468170.00	27/06/2014	10:17:14	9793899.63	0.11	40269
1	403387.00	6468170.00	27/06/2014	10:18:20	9793899.73	0.11	40269
2	410153.00	6467499.00	27/06/2014	10:45:59	9794484.12	0.11	40269
2	410153.00	6467499.00	27/06/2014	10:47:05	9794484.19	0.11	40269
1	403387.00	6468170.00	27/06/2014	11:11:09	9793899.66	0.11	40269
1	403387.00	6468170.00	27/06/2014	11:12:15	9793899.63	0.11	40269
1	403387.00	6468170.00	27/06/2014	11:12:15	9793899.63	0.25	40269
2	410153.00	6467499.00	27/06/2014	11:39:40	9794483.98	0.25	40269
2	410153.00	6467499.00	27/06/2014	11:40:46	9794483.95	0.25	40269
1	403387.00	6468170.00	27/06/2014	12:05:34	9793899.63	0.25	40269
1	403387.00	6468170.00	27/06/2014	12:06:40	9793899.63	0.25	40269
1	403387.00	6468170.00	27/06/2014	12:06:40	9793899.63	0.28	40269
2	410153.00	6467499.00	27/06/2014	12:33:10	9794484.02	0.28	40269
2	410153.00	6467499.00	27/06/2014	12:34:16	9794484.09	0.28	40269
1	403387.00	6468170.00	27/06/2014	13:00:16	9793899.61	0.28	40269
1	403387.00	6468170.00	27/06/2014	13:01:22	9793899.63	0.28	40269
<b>AVG2</b>					<b>9794484.06</b>		

P2014065\_GA\_Gippsland

**Post Survey Calibration Data**

1 = 2010990117 CS1 Guildford Cemetery 9793899.63  $\mu\text{m/s}^2$  AAGD07

2 = 2010990217 CS2 Helena Valley Primary School 9794483.85  $\mu\text{m/s}^2$  AAGD07

Station	MGAE	MGAN	Date	Time	OBSGAAD07_ $\mu\text{m/s}^2$	Drift_ $\mu\text{m/s}^2$	Serial
A3 METER							
1	403387.00	6468170.00	12/09/2014	9:33:31	9793899.63	0.07	40269
1	403387.00	6468170.00	12/09/2014	9:34:37	9793899.62	0.07	40269
2	410153.00	6467499.00	12/09/2014	10:13:35	9794484.18	0.07	40269
2	410153.00	6467499.00	12/09/2014	10:14:41	9794484.18	0.07	40269
1	403387.00	6468170.00	12/09/2014	10:48:58	9793899.63	0.07	40269
1	403387.00	6468170.00	12/09/2014	10:50:04	9793899.63	0.07	40269
1	403387.00	6468170.00	12/09/2014	10:50:04	9793899.63	0.07	40269
2	410153.00	6467499.00	12/09/2014	11:22:54	9794484.21	0.07	40269
2	410153.00	6467499.00	12/09/2014	11:24:00	9794484.20	0.07	40269
1	403387.00	6468170.00	12/09/2014	11:58:11	9793899.64	0.07	40269
1	403387.00	6468170.00	12/09/2014	11:59:17	9793899.63	0.07	40269
<b>AVG2</b>					<b>9794484.19</b>		

# Appendix D - Repeat gravity data

## Repeat Listing: All Observations

Station	MGAEast	MGANorth	Repeat_error elevation_m	Repeat_error gravity_μm/s <sup>2</sup>	Date_ ddmmyy	Time_ hhmmss	Metersn
20140101371	397277.6	5745579.7	0.045	0.24	02072014	080251	40269
20140102157	392639.1	5741005.2	-0.111	-0.03	02072014	130952	40269
20140101395	405368.9	5737736.7	0.019	0.43	02072014	165336	40269
20140101386	401990.1	5739859.4	-0.012	0.04	02072014	170609	40269
20140101370	397134.2	5746060.4	-0.028	-0.07	02072014	172024	40269
20140101371	397278.0	5745580.5	0.082	-0.32	03072014	073132	40269
20140101386	401987.5	5739858.4	-0.003	0.00	03072014	075543	40269
20140101395	405369.0	5737737.0	0.043	-0.23	03072014	080552	40269
20140102178	399117.7	5731288.5	0.070	-0.29	03072014	081511	40269
20140101370	397134.4	5746060.1	0.017	-0.35	03072014	173300	40269
20140101386	401989.9	5739860.1	-0.015	0.03	04072014	074833	40269
20140101395	405368.6	5737737.9	0.004	0.08	04072014	081355	40269
20140102178	399116.6	5731286.1	0.018	0.00	04072014	082243	40269
20140101212	396747.4	5727635.7	-0.078	0.21	04072014	083029	40269
20140101219	398081.3	5723737.8	-0.054	0.07	04072014	083938	40269
20140102235	399508.1	5722908.6	-0.060	0.33	04072014	084527	40269
20140102253	407942.9	5732764.1	-0.089	0.37	04072014	143931	40269
20140102248	404747.6	5731107.0	0.027	0.21	04072014	144655	40269
20140102235	399508.3	5722909.1	0.059	0.46	04072014	151351	40269
20140101370	397134.3	5746060.2	-0.013	-0.27	05072014	072508	40269
20140101013	366795.3	5732340.6	-0.041	-0.45	05072014	141847	40269
20140101372	397482.0	5745179.8	-0.002	0.66	06072014	072758	40269
20140101386	401988.2	5739858.8	-0.016	0.21	06072014	074043	40269
20140101395	405368.9	5737736.6	-0.030	0.09	06072014	074953	40269
20140102253	407942.9	5732764.0	0.050	-0.21	06072014	080139	40269
20140102414	434518.1	5699534.1	-0.049	-0.09	06072014	141457	40269
20140102403	429664.6	5705074.1	0.053	-0.48	06072014	142347	40269
20140101459	424758.7	5710684.0	0.027	0.01	06072014	143322	40269
20140101445	419820.0	5716720.7	0.014	0.27	06072014	154815	40269
20140101372	397482.0	5745179.8	0.003	0.10	07072014	072136	40269
20140101386	401988.2	5739858.6	0.029	-0.04	07072014	073455	40269
20140101395	405369.1	5737737.4	-0.030	-0.42	07072014	074539	40269
20140102253	407942.7	5732763.8	0.029	0.27	07072014	082232	40269
20140102208	412113.1	5716065.8	0.045	-0.20	07072014	103022	40269
20140101445	419820.4	5716720.8	-0.001	-0.14	07072014	105755	40269
20140101372	397482.0	5745179.8	0.045	0.23	08072014	073316	40269
20140101371	397277.4	5745579.3	-0.002	0.04	08072014	073733	40269
20140101370	397134.4	5746060.4	0.010	0.30	08072014	074525	40269
20140102157	392643.1	5741008.9	0.055	0.05	08072014	075822	40269
20140101189	386738.1	5735897.6	-0.032	-0.11	08072014	080957	40269
20140101087	383417.6	5732418.8	-0.041	-0.02	08072014	081949	40269
20140101077	378227.2	5737690.3	0.020	-0.09	08072014	091547	40269

Station	MGAEast	MGANorth	Repeat_error elevation_m	Repeat_error gravity_μm/s <sup>2</sup>	Date_ ddmmyy	Time_ hhmmss	Metersn
20140102076	386056.9	5746819.3	0.057	0.26	08072014	162304	40269
20140101370	397134.8	5746060.4	-0.033	0.08	08072014	164204	40269
20140101372	397482.0	5745179.8	0.002	-0.09	09072014	080622	40269
20140101371	397277.3	5745579.3	0.008	0.60	09072014	081010	40269
20140101370	397134.7	5746060.4	-0.008	0.33	09072014	081358	40269
20140102157	392642.8	5741008.5	0.028	0.41	09072014	082521	40269
20140101189	386738.3	5735897.6	-0.021	0.25	09072014	083641	40269
20140102070	383839.6	5744395.8	0.011	0.00	09072014	093412	40269
20140102068	382728.5	5743309.6	-0.028	0.14	09072014	093929	40269
20140101160	376849.6	5749552.1	0.000	0.34	09072014	104603	40269
20140101161	377376.6	5749569.5	-0.104	0.03	09072014	105322	40269
20140102127	381904.3	5754492.9	0.026	0.13	09072014	131821	40269
20140102095	391644.1	5754241.7	-0.024	0.21	09072014	141141	40269
20140101372	397482.1	5745179.8	0.052	-0.18	10072014	072109	40269
20140101371	397277.5	5745579.4	-0.009	-0.17	10072014	072513	40269
20140101370	397134.6	5746060.3	0.003	0.14	10072014	072926	40269
20140101352	393788.6	5754302.3	-0.035	-0.28	10072014	074943	40269
20140101349	392165.2	5755387.0	0.021	-0.35	10072014	075438	40269
20140101349	392165.7	5755387.1	-0.019	-0.36	10072014	151140	40269
20140101370	397134.6	5746060.4	0.014	0.30	10072014	170604	40269
20140101372	397482.1	5745179.7	-0.033	0.19	11072014	072701	40269
20140102253	407942.9	5732764.0	-0.022	-0.11	11072014	075014	40269
20140102351	424818.4	5725781.2	-0.013	0.54	11072014	083135	40269
20140101371	397277.2	5745579.1	-0.030	-0.14	12072014	075006	40269
20140102351	424818.3	5725781.7	0.014	-0.68	12072014	083348	40269
20140101592	432151.2	5729677.2	-0.034	-0.33	12072014	090408	40269
20140101395	405368.8	5737737.0	0.011	0.31	12072014	170048	40269
20140101386	401990.5	5739859.4	0.023	0.00	12072014	171028	40269
20140101372	397482.2	5745179.8	0.016	-0.17	13072014	072602	40269
20140101371	397277.1	5745579.0	-0.056	-0.17	13072014	073000	40269
20140101370	397134.6	5746060.4	0.003	-0.36	13072014	073413	40269
20140101789	408393.8	5788642.2	0.123	0.45	13072014	154624	40269
20140101372	397482.1	5745179.7	0.016	-0.15	15072014	073510	40269
20140101386	401988.2	5739859.1	0.011	0.03	15072014	074652	40269
20140102270	412374.5	5739364.0	0.039	-0.09	15072014	080100	40269
20140101624	397554.6	5783607.9	-0.066	-0.07	15072014	131049	40269
20140101650	406031.2	5773254.3	-0.018	0.34	15072014	151347	40269
20140101370	397134.7	5746060.3	0.003	-0.14	15072014	165748	40269
20140101371	397277.2	5745579.1	-0.020	-0.10	15072014	170231	40269
20140101372	397482.0	5745179.7	0.016	-0.06	16072014	071846	40269
20140101371	397277.0	5745579.0	-0.033	-0.05	16072014	072305	40269
20140101386	401988.5	5739859.1	0.000	0.00	16072014	073616	40269
20140101550	414920.5	5744285.0	-0.028	0.11	16072014	075417	40269
20140101701	425722.9	5749586.4	0.022	-0.17	16072014	080836	40269
20140101665	413375.1	5764204.8	0.002	-0.02	16072014	135913	40269
20140101701	425723.2	5749586.3	0.014	-0.31	16072014	165339	40269
20140101550	414920.0	5744284.9	0.037	-0.22	16072014	171547	40269
20140101372	397482.1	5745179.5	-0.027	0.08	17072014	072755	40269



Station	MGAEast	MGANorth	Repeat_error elevation_m	Repeat_error gravity_μm/s <sup>2</sup>	Date_ ddmmyy	Time_ hhmmss	Metersn
20140101371	397277.0	5745578.9	-0.013	0.19	17072014	074344	40269
20140101550	414920.4	5744284.7	-0.026	0.25	17072014	080504	40269
20140101701	425722.7	5749586.5	-0.013	0.33	17072014	081846	40269
20140101822	432065.1	5756741.9	-0.028	0.12	17072014	083110	40269
20140101934	434526.5	5780234.5	0.056	-0.01	17072014	115800	40269
20140101942	435424.9	5776080.3	0.006	0.25	17072014	120509	40269
20140101372	397482.1	5745179.5	0.016	-0.15	18072014	071749	40269
20140101550	414920.3	5744284.8	-0.002	-0.07	18072014	073918	40269
20140101701	425722.8	5749586.3	-0.049	-0.33	18072014	075413	40269
20140101763	451140.8	5720600.1	-0.076	0.15	18072014	171113	40269
20140101372	397481.9	5745179.6	0.021	-0.19	19072014	072442	40269
20140102253	407943.2	5732763.9	0.023	-0.30	19072014	075432	40269
20140102351	424818.5	5725781.2	0.000	-0.41	19072014	081338	40269
20140101763	451140.9	5720600.3	0.008	0.00	19072014	090906	40269
20140101837	436416.2	5751707.8	-0.013	0.25	19072014	170106	40269
20140101701	425723.0	5749586.6	-0.013	0.43	19072014	172608	40269
20140101371	397276.9	5745579.4	0.040	0.01	20072014	072536	40269
20140102270	412374.1	5739363.9	-0.055	0.02	20072014	074500	40269
20140101701	425722.8	5749586.4	0.000	-0.01	20072014	082830	40269
20140101837	436416.1	5751707.0	0.017	0.01	20072014	095446	40269
20140102351	424818.5	5725781.6	0.024	-0.17	20072014	144304	40269
20140101372	397481.9	5745179.4	-0.015	-0.30	21072014	074212	40269
20140101371	397277.2	5745579.3	-0.003	0.07	21072014	074612	40269
20140101650	406031.4	5773254.3	-0.041	-0.28	21072014	091814	40269
20140101763	451140.8	5720600.2	-0.045	-0.25	21072014	135844	40269
20140102253	407942.4	5732763.7	-0.029	-0.16	21072014	152408	40269
20140102248	404748.8	5731105.9	-0.117	-0.20	21072014	153026	40269
20140101395	405368.9	5737737.4	-0.018	0.09	21072014	154624	40269
20140101386	401990.6	5739859.2	-0.010	0.06	21072014	155618	40269
20140101370	397134.7	5746060.1	0.004	-0.16	21072014	160936	40269

# Appendix E - Longman's earth tide correction formula

```
input dLat (latitude)
input dLon (longitude)
input dDate (date)
*Date broken down into year, month and date
input dTime (time)

array pClnr[12]={0,31,59,90,120,151,181,212,243,273,304,334}
lYr=year
lMo=month
lDa=day

ny=(lYr-1900)
days=(dTime/24.0+lDa-1+pClnr[lMo-1])
lLeap=(ny/4)
if (lLeap/2=ny and lMo<3) then lLeap=lLeap-1
lDay=(ny*365+lLeap+lDa+pClnr[lMo-1])
dcent = (ny*365.0+lLeap+days+0.5)/36525)
dhrs = (ny*365.0+lLeap+days+0.5)*24.0)
ds = (dcent*8399.709299+4.720023434+(dcent*dcent)*4.40696e-5)
dp=(dcent*71.01800936+5.835124713-(dcent*dcent)*1.80545e-4-dcent*2.1817e-7*(dcent*dcent))
dh=(dcent*628.3319509+4.88162792+(dcent*dcent)*5.27962e-6)
doln=(4.523588564-dcent*33.757153303+(dcent*dcent)*3.6749e-5)
dps=(dcent*0.03000526416+4.908229461+(dcent*dcent)*7.902463e-6)
des=(0.01675104-dcent*4.18e-5-(dcent*dcent)*1.26e-7)
dsoln=(sin(doln))
dci=(0.91369-cos(doln))*0.03569)
dsi=(sqrt(1.0-(dci*dci)))
dsn=(dsoln*0.08968/dsi)
dcn=(sqrt(1.0-(dsn*dsn)))
dtit=(dsoln*0.39798/(dsi*cos(doln)*dcn+1.0dsoln*0.91739*dsn))
det=(atan(dtit)*2.0)
if (det<0.0)then det=det+6.2831852)

dolm1=(ds-doln+det+sin(ds-dp)*0.10979944)
dolm=(dolm1+sin((ds-dp)*2.0)*0.003767474+sin(ds-dh*2.0+dp)*0.0154002+sin((ds-dh)*2.0)*0.00769395)
dha=((dTime*15.0-180)*0.0174532925199+dLon/57.295779513)
dchi=(dha+dh-atan(dsn/dcn))
dal=(dLat/57.295779513)
dct=(sin(dal)*dsi*sin(dolm)+cos(dal)*((dci+1.0)*cos(dolm-dchi)+(1.0-dci)*cos(dolm+dchi))/2.0)
dda=(cos(ds-dp)*0.14325+2.60144+cos((ds-dp)*2.0)*0.0078644+cos(ds-dh*2.0+dp)*0.0200918+cos((ds-dh)*2.0)*0.0146006)
dr=(6.378388/sqrt((1.0-(cos(dal)*cos(dal))*0.00676902+1.0))
r_1=(dda)
r_2=(dct)
r_3=(dr)
r_4=(dda)
r_5=(dda*dda)
r_6=(dct)
dgm=(dr80.49049*dda*(r_1*r_1)*((r_2*r_2)*3.0-1.0)+(r_3*r_3)*7.4e-4*(r_5*r_5)*dct*((r_6*r_6)*5.0-3.0))
dols=(dh+des*2.0*sin(dh-dps))
dchis=(dha+dh)
dds=((des*cos(dh-dps)+1.0)*0.668881/(1.0-(des*des)))
dcf=(sin(dal)*0.39798*sin(dols)+cos(dal)*cos(dols-
```

# Appendix F - Data formats and metadata

```
DEFN ST=RECD,RT=COMM;RT:A4;COMMENTS:A76
DEFN 1 ST=RECD,RT=;PROJECT:F7.0:NULL=-9999.,UNIT=None,NAME=PROJECT
DEFN 2 ST=RECD,RT=;STATION:F12.0:NULL=-999999999.,UNIT=None,NAME=STATION
DEFN 3 ST=RECD,RT=;LATITUDE:F11.6:NULL=-99.999999,UNIT=Decimal Degrees,NAME=LATITUDE
DEFN 4 ST=RECD,RT=;LONGITUDE:F12.6:NULL=-999.999999,UNIT=Decimal Degrees,NAME=LONGITUDE
DEFN 5 ST=RECD,RT=;EASTING:F9.1:NULL=-99999.9,UNIT=metres,NAME=EASTING
DEFN 6 ST=RECD,RT=;NORTHING:F10.1:NULL=-999999.9,UNIT=metres,NAME=NORTHING
DEFN 7 ST=RECD,RT=;ELLIPSHTEGRS80:F9.3:NULL=-999.999,UNIT=metres,NAME=ELLIPSHTEGRS80
DEFN 8 ST=RECD,RT=;NAG09:F9.3:NULL=-999.999,UNIT=metres,NAME=NAG09
DEFN 9 ST=RECD,RT=;GRNDELEVATION:F9.3:NULL=-999.999,UNIT=metres,NAME=GRNDELEVATION
DEFN 10 ST=RECD,RT=;OBSSGAAGD07:F12.2:NULL=-9999999.99,UNIT= $\mu\text{m/s}^2$ ,NAME=OBSSGAAGD07
DEFN 11 ST=RECD,RT=;HTGM:F9.3:NULL=-999.999,UNIT=metres,NAME=HTGM
DEFN 12 ST=RECD,RT=;TCINNER:F7.2:NULL=-99.99,UNIT= $\mu\text{m/s}^2$ ,NAME=TCINNER
DEFN 13 ST=RECD,RT=;TCQFINNER:I4:NULL=-99,UNIT=None,NAME=TCQFINNER
DEFN 14 ST=RECD,RT=;TCOUTER:F7.2:NULL=-99.99,UNIT= $\mu\text{m/s}^2$ ,NAME=TCOUTER
DEFN 15 ST=RECD,RT=;TCQFOUTER:I4:NULL=-99,UNIT=None,NAME=TCQFOUTER
DEFN 16 ST=RECD,RT=;TCTOTAL:F7.2:NULL=-99.99,UNIT= $\mu\text{m/s}^2$ ,NAME=TCTOTAL
DEFN 17 ST=RECD,RT=;EFAA:F10.2:NULL=-99999.99,UNIT= $\mu\text{m/s}^2$ ,NAME=EFAA
DEFN 18 ST=RECD,RT=;SCBA267:F10.2:NULL=-99999.99,UNIT= $\mu\text{m/s}^2$ ,NAME=SCBA267
DEFN 29 ST=RECD,RT=;CSCBA267:F10.2:NULL=-99999.99,UNIT= $\mu\text{m/s}^2$ ,NAME=CSCBA267
DEFN 20 ST=RECD,RT=;HORIZDIST:F9.2:NULL=-9999.99,UNIT=metres,NAME=HORIZDIST
DEFN 21 ST=RECD,RT=;GRVBASE:F13.0:NULL=-9999999999.,UNIT=None,NAME=GRVBASE
DEFN 22 ST=RECD,RT=;GPSBASE:F13.0:NULL=-9999999999.,UNIT=None,NAME=GPSBASE
DEFN 23 ST=RECD,RT=;TIME:A9;UNIT=None,NAME=TIME
DEFN 24 ST=RECD,RT=;DATE:A9;UNIT=None,NAME=DATE
DEFN 25 ST=RECD,RT=;MGAZONE:F4.0:NULL=-9.,UNIT=None,NAME=MGAZONE
DEFN 26 ST=RECD,RT=;GMTYPESN:A30;UNIT=None,NAME=GMTYPESN
DEFN 27 ST=RECD,RT=;STATIONDESC:F20.0:NULL=-99.,UNIT=None,NAME=STATIONDESC;END DEFN
DEFN 29 ST=RECD,RT=;COMMENTS:F20.0:NULL=-99.,NAME=COMMENTS;END DEFN
DEFN 1 ST=RECD,RT=PROJ; RT:A4
DEFN 2 ST=RECD,RT=PROJ; PROJNAME:A30: COMMENT=GDA94 / MGA zone 55
DEFN 3 ST=RECD,RT=PROJ; ELLPSNAM:A30: COMMENT=GRS 1980
DEFN 4 ST=RECD,RT=PROJ; MAJ_AXIS: D12.1: UNIT=m, COMMENT=6378137.000000
DEFN 5 ST=RECD,RT=PROJ; ECCENT: D12.9: COMMENT=298.257222
DEFN 6 ST=RECD,RT=PROJ; PRIMEMER: F10.1: UNIT=deg, COMMENT=0.000000
DEFN 7 ST=RECD,RT=PROJ; PROJMETHOD: A30: COMMENT=Transverse Mercator
DEFN 8 ST=RECD,RT=PROJ; PARAM1: D14.0: COMMENT= 0.000000
DEFN 9 ST=RECD,RT=PROJ; PARAM2: D14.0: COMMENT= 147.000000
DEFN 10 ST=RECD,RT=PROJ; PARAM3: D14.0: COMMENT= 0.999600
DEFN 11 ST=RECD,RT=PROJ; PARAM4: D14.0: COMMENT= 500000.000000
DEFN 12 ST=RECD,RT=PROJ; PARAM5: D14.0: COMMENT=10000000.000000
DEFN 13 ST=RECD,RT=PROJ; PARAM6: D14.0:
DEFN 14 ST=RECD,RT=PROJ; PARAM7: D14.0:
DEFN 15 ST=RECD,RT=PROJ; END DEFN
```

COMM ATLAS GEOPHYSICS PTY LTD ASEG-GDF2 FORMAT FILE  
 COMM WWW.ATLASGEO.COM.AU  
 COMM INFO@ATLASGEO.COM.AU  
 COMM  
 COMM ATLAS PROJECT NUMBER P2014065  
 COMM GA PROJECT NUMBER 201430  
 COMM CLIENT GA  
 COMM PROJECT AREA GIPPSLAND GRAVITY SURVEY  
 COMM START DATE 01072014  
 COMM END DATE 21072014  
 COMM PROCESSED BY LR MATHEWS  
 COMM  
 COMM VESSEL VEHICLE  
 COMM OPERATORS GEOSCIENCE AUSTRALIA / GA  
 COMM OBSERVERS ZS,WB  
 COMM  
 COMM MIN SPACING 500m  
 COMM MAX SPACING 500m  
 COMM LAYOUT TRAVERSE  
 COMM  
 COMM GRAVITY STATIONS 1213  
 COMM  
 COMM GEODETIC DATUM GDA94  
 COMM PROJECTION MGA55  
 COMM HORIZ ACCURACY 0.05 m  
 COMM  
 COMM VERTICAL DATUM GRS80  
 COMM VERTICAL ACCURACY 0.08 m  
 COMM  
 COMM GRAVITY DATUM AAGD07  
 COMM GRAVITY ACCURACY 0.25  $\mu\text{m/s}^2$   
 COMM  
 COMM GRAVITY INSTRUMENT SCINTREX CG5  
 COMM GRAVITY SN 40269  
 COMM GPS INSTRUMENT LEICA GS14  
 COMM GPS METHOD RTK  
 COMM  
 COMM GPS BASE 20143000001 (VRS BASES)  
 COMM GRV BASE 20143000001  
 COMM CTRL TIE STATION 1995901324,1995909324  
 COMM  
 COMM PROCESSING  
 COMM DRIFT CORRECTION  
 COMM ETC CORRECTION LONGMAN  
 COMM NORMAL GRAVITY  $9780326.7715 * ((1 + 0.001931851353 * (\sin(B3 * (\pi / 180))))^2) / (\sqrt{(1 - 0.0066943800229 * (\sin(B3 * (\pi / 180))))^2}))$   
 COMM ATMOSPHERIC CORRECTION  $8.74 - 0.00099 * F3 + 0.0000000356 * F3^2$   
 COMM FREE AIR CORRECTION  $-(3.087691 - 0.004398 * \sin(\text{LAT})^2) * \text{ELLIPSH T} + 0.00000072125 * \text{ELLIPSH T}^2$

COMM SCAP BOUGUER CORRECTION	$2 \cdot \pi \cdot G_p \cdot (1 + \mu) \cdot \text{ELLIPSHT-LAMBDA} \cdot R$ for $p=2.67 \text{ t/m}^3$	
COMM TERRAIN CORRECTION METHOD	RASTERTC	
COMM		
COMM SOFTWARE	AGRIS(IN HOUSE), WAYPOINT850, CHRISDBF, ERMAPPER, RASTERTC	
COMM		
COMM		
COMM DETAILED COLUMN DESCRIPTIONS		
COMM COLUMN NAME	COLUMN DESCRIPTION	UNITS
COMM		
COMM PROJECT	GA PROJECT NUMBER NONE	
COMM STATION	GA STATION NUMBER NONE	
COMM LATITUDE	COORDINATE LATITUDE GDA94	DECIMAL DEGREES
COMM LONGITUDE	COORDINATE LONGITUDE GDA94	DECIMAL DEGREES
COMM EASTING	COORDINATE EASTING MGA/GDA94	M
COMM NORTHING	COORDINATE NORTHING MGA/GDA94	M
COMM ELLIPSHTGRS80	COORDINATE ELEVATION ELLIPSOIDAL GRS80	M
COMM NAG09	GEOID ELLIPSOID SEPARATION AUSGEOID09	M
COMM GRNDELEVATION	GROUND LEVEL ELEVATION	M
COMM OBSGAAGD07GU	OBSERVED GRAVITY AAGD07	$\mu\text{m/s}^2$
COMM HTGM	STATION HEIGHT OF GRAVITY METER	M
COMM TCINNER267	INNER ZONE TERRAIN CORRECTION $2.67 \text{ t/m}^3$	$\mu\text{m/s}^2$
COMM TCQFINNER	QUALITY FACTOR OF INNER ZONE TERRAIN CORRECTION	NONE
COMM TCOUTER267	OUTER ZONE TERRAIN CORRECTION $2.67 \text{ t/m}^3$	$\mu\text{m/s}^2$
COMM TCQFOUTER	QUALITY FACTOR OF OUTER ZONE TERRAIN CORRECTION	NONE
COMM TCTOTAL267	TOTAL TERRAIN CORRECTION $2.67 \text{ t/m}^3$	$\mu\text{m/s}^2$
COMM EFAA	ELLIPSOIDAL FREE AIR ANOMALY	$\mu\text{m/s}^2$
COMM SCBA267	SPHERICAL CAP BOUGUER ANOMALY $2.67 \text{ t/m}^3$	$\mu\text{m/s}^2$
COMM CSCBA267	COMPLETE SPHERICAL CAP BOUGUER ANOMALY $2.67 \text{ t/m}^3$	$\mu\text{m/s}^2$
COMM HORIZDIST	HORIZONTAL DISTANCE FROM PROGRAMMED STATION	M
COMM GRVBASE	GRAVITY BASE STATION REFERENCED TO	NONE
COMM GPSBASE	GPS BASE STATION REFERENCED TO	NONE
COMM TIME	TIME OF GRAVITY OBSERVATION	NONE
COMM DATE	DATE OF GRAVITY OBSERVATION	NONE
COMM MGAZONE	MGA ZONE NUMBER	NONE
COMM GMTYPESN	GRAVITY METER TYPE SERIAL	NONE
COMM STATIONDESC	STATION DESC	NONE
COMM COMMENTS	COMMENTS	NONE





the 1990s, the number of people in the world who are illiterate has increased from 1.2 billion to 1.5 billion.

There are many reasons for this. One is that the population of the world is growing. Another is that the number of people who are illiterate is increasing in many countries, particularly in the developing world. This is because of a number of factors, including a lack of access to education, a lack of resources, and a lack of political will.

One of the main reasons for the increase in illiteracy is the lack of access to education. In many developing countries, there are not enough schools, and the quality of education is poor. This means that many children do not go to school, and those who do often do not learn to read and write.

Another reason for the increase in illiteracy is the lack of resources. In many developing countries, there is a lack of money to invest in education. This means that there are not enough teachers, and the schools are often overcrowded. This makes it difficult for children to learn.

A third reason for the increase in illiteracy is the lack of political will. In many developing countries, the government does not prioritize education. This means that there is not enough money invested in education, and the quality of education is poor. This makes it difficult for children to learn.

There are many ways to reduce the number of illiterate people in the world. One way is to increase access to education. This can be done by building more schools, and by improving the quality of education. Another way is to increase resources for education. This can be done by increasing the amount of money invested in education, and by recruiting more teachers.

Finally, it is important to have political will to prioritize education. This means that the government must invest in education, and must ensure that the quality of education is high.

By doing these things, we can reduce the number of illiterate people in the world, and we can help to create a better future for all.

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By doing these things, we can reduce the number of illiterate people in the world, and we can help to create a better future for all. This is a goal that we should all strive for, and it is one that we can achieve if we work together.

There are many ways to reduce the number of illiterate people in the world. One way is to increase access to education. This can be done by building more schools, and by improving the quality of education. Another way is to increase resources for education. This can be done by increasing the amount of money invested in education, and by recruiting more teachers.

A third way to reduce the number of illiterate people is to increase political will. This means that the government must invest in education, and must ensure that the quality of education is high. This can be done by increasing the amount of money invested in education, and by recruiting more teachers.

By doing these things, we can reduce the number of illiterate people in the world, and we can help to create a better future for all. This is a goal that we should all strive for, and it is one that we can achieve if we work together.